

The nephron: loop of Henle

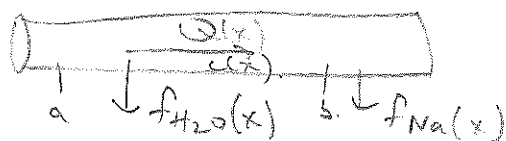
Function of kidney is to regulate composition of blood plasma (part of blood left over with remainder). Goal of this chapter: model regulation of Na^+ concentration in the plasma.

Basic unit of kidney: the nephron. Kidney has 10^6 nephrons arranged in parallel.

Details in book: the summary - that the changes in Na^+ concentration occur in the loop of Henle, which will be our modelling focus.

Dynamics of transport

Consider steady flow through a tube



f = flux per unit length
 Q = flow rate

Mass balance of water

$$Q(a) - Q(b) = \int_a^b f_{\text{H}_2\text{O}}(x) dx$$

Now differentiate w.r.t. b

$$-Q'(b) = f_{\text{H}_2\text{O}}(b)$$

Since b is arbitrary, get

$$0 = Q' + f$$

$$0 = \frac{dQ}{dx} + f_{\text{H}_2\text{O}}$$

If $f=0$, Q is constant

Now consider transport of Na^+ . Mass balance between a

and b gives

$$c(a)Q(a) - c(b)Q(b) = \int_a^b f_{\text{Na}}(x) dx$$

and so the argument is the same with cQ replacing Q .

The resulting ODE is

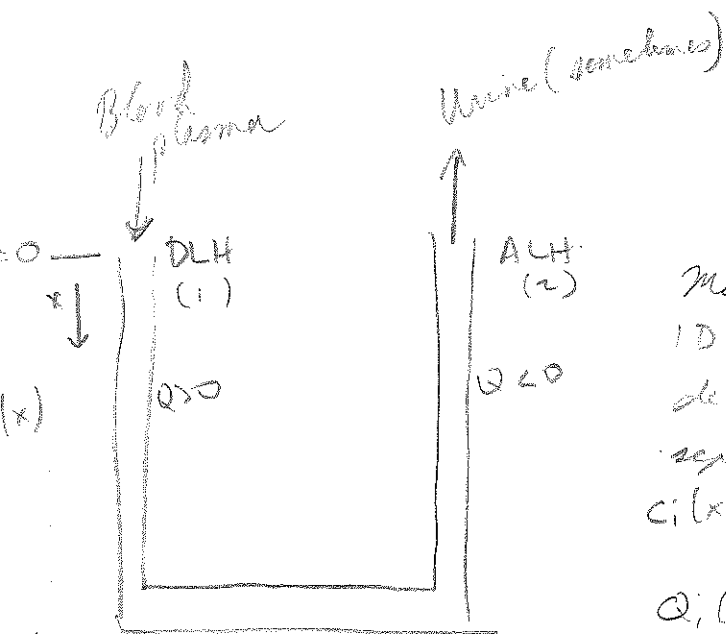
$$0 = \frac{d}{dx}(cQ) + f_{\text{Na}}$$

When $f_{\text{Na}}=0$, cQ is constant.

We will apply these equations to the different structures in the kidney.

The loop of Henle

As a subunit in the kidney the job of the loop is to remove Na^+ and water from the tubular fluid that enters it. The fluid leaving Henle-loop eventually becomes urine.



Model of loop of Henle.

1D model where we consider the descending and ascending loop separately.

$c_i(x)$ = concentration in tube i
 $i = 1, 2$

$Q_i(x)$ = water flow rate

Let $c(x)$ = external sodium concentration

Physiological assumptions + model

1) The descending limb is permeable to water but not Na^+ . Permeability is large enough to equilibrate internal + external concentrations:

$$c_1(x) = c(x)$$

$$0 = \frac{d}{dx} (c_1 Q_1)$$

$$\frac{dQ_1}{dx} + f_{\text{H}_2\text{O}}(x) = 0$$

2) Na^+ is pumped out of ascending limb at fixed rate f_{Na}^* . Assume ascending limb impermeable to water.

$$\frac{dQ_2}{dx} = 0$$

$$\frac{d}{dx} (c_2 Q_2) + f_{\text{Na}}^* = 0$$

3) at join of the loop assume continuity of ascending + descending limb

$$c_1(L) = c_2(L)$$

$$Q_1(L) = -Q_2(L)$$

4) Consider the other part of the kidney, called the peritubular capillaries that picks up sodium and water. In our model, rate of sodium pick up from ascending limb = f_{Na}^* , while the rate of water pick up from descending limb is $f_{\text{H}_2\text{O}}^{(1)}$. But the sodium must come through the water! So

$$f_{\text{Na}}^* = f_{\text{H}_2\text{O}}^{(1)}(x) c(x)$$

Let us derive an ODE for $c(x)$ from

$$0 = \frac{dQ_1}{dx} + f_{Na}^* = \frac{dQ_1}{dx} + \frac{f_{Na}^*}{c} \rightarrow c \frac{dQ_1}{dx} + f_{Na}^* = 0$$

But we know sodium is conserved in the descending loop

$$\frac{d}{dx} (cQ_1) = 0 \rightarrow Q_1(x)c(x) = Q_1(0)c(0)$$

$$Q_1(x) = \frac{Q_1(0)c(0)}{c(x)}$$

So $c(x) Q_1(0) c(0) \frac{d}{dx} \left(\frac{1}{c(x)} \right) + f_{Na}^* = 0$

$$= \cancel{c(x) Q_1(0) c(0)} - \frac{1}{c(x)} \frac{dc}{dx} + f_{Na}^* = 0$$

important to take

$$\frac{dc}{dx} = \frac{f_{Na}^* c(x)}{Q_1(0)c(0)}$$

Exercise: Solve this for $c(x)$.

$$c(x) = c(0) \exp\left(\frac{f_{Na}^* x}{Q_1(0)c(0)}\right)$$

So $c(L) = c(0) \exp\left(\frac{f_{Na}^* L}{Q_1(0)c(0)}\right)$

Note that $f_{Na}^* L =$ rate at which Na^+ is pumped out through ALH.
 $Q_1(0)c(0) =$ total rate at which Na^+ enter TALH.

So $\alpha = \frac{f_{Na}^* L}{Q_1(0)c(0)} < 1$.

determine concentrating ability of nephron through eq.

$$c(L) = c(0) \exp(\alpha)$$

Now ready to look at ascending limb (Na^+ pumped in).

$$Q_2(x) = Q_2(L) = -Q_1(L) = -\frac{Q_1(0)c(0)}{c(L)} = -Q_1(0) \exp(-\alpha)$$

Since Q_2 is constant, the sodium eqn

$$0 = \frac{d}{dx} (Q_2 c_2) + f_{Na}^*$$

hence

$$Q_2 \frac{dc_2}{dx} = -f_{Na}^* \Rightarrow \frac{dc_2}{dx} = \frac{f_{Na}^* \exp(\alpha)}{Q_1(0)}$$

Exercise Solve this ODE $c_2(L) = c(L)$

$$c_2(x) = c_2(L) + \frac{f_{Na}^* \exp(\alpha)}{Q_1(0)} (x-L)$$

But by continuity

$$c_2(L) = c_1(L) = c(L) = c(0) \exp(\alpha) \quad \text{So}$$
$$c_2(x) = c(L) \exp(\alpha) + (x-L) \frac{N_a \exp(\alpha)}{\omega_1(0)}$$

$$\text{and } c_2(0) = c(0) \exp(\alpha) - \frac{L N_a \exp(\alpha)}{\omega_1(0)} \quad c(0)$$
$$= c(0) \left[\exp(\alpha) - \alpha \exp(\alpha) \right]$$
$$= c(0) \exp(\alpha) (1 - \alpha)$$

When $\alpha \neq 0$, $\exp(\alpha)(1 - \alpha) < 1$. So $c_2(0) < c(0)$.

Fluid leaving ACH is more dilute than fluid plasma

Do we want this and how can we control it? Several times.