Axis-Aligned Height-Field Block Decomposition of 3D Shapes

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We propose a novel algorithm for decomposing general 3D geometries into a small set of overlap-free height-field blocks, volumes enclosed by a flat base and a height-field surface defined along a direction orthogonal to, and located strictly above, this base. This decomposition is useful for fabrication methodologies such as 3-axis CNC milling, where a single milling pass can only carve a single height-field surface defined with respect to the machine tray, but can also benefit other fabrication settings. Computing our desired decomposition requires solving a highly constrained discrete optimization problem, variants of which are known to be NP-hard. We effectively compute a high-quality decomposition by using a two-step process that leverages the unique characteristics of our setup. Specifically, we notice that if the height-field directions are constrained to the major axes we can always produce a valid decomposition starting from a suitable surface segmentation. Our method first produces a compact set of large, possibly overlapping, height-field blocks that jointly cover the model surface by recasting this discrete constrained optimization problem as an unconstrained optimization of a continuous function, which allows for an efficient solution. We then cast the computation of an overlap-free, final decomposition as an ordering problem on a graph, and solve it via a combination of cycle elimination and topological sorting. The combined algorithm produces a compact set of height-field blocks that jointly describe the input model within a user given tolerance. We demonstrate our method on a range of inputs, and showcase a number of real life models manufactured using our technique.

CCS Concepts: • Computing methodologies → Mesh models; Mesh geometry models;

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1 INTRODUCTION
The advent of digital manufacturing has opened the doors to broad-based bespoke 3D object fabrication, while simultaneously introducing numerous new geometry processing challenges. Fabrication often requires decomposing the processed shapes into blocks that satisfy different sets of geometric requirements [Livesu et al. 2017; Medeiros e Sá et al. 2016]. Our work addresses one of the most challenging decomposition problems that arise in fabrication settings: height-field block decomposition. Height-field blocks are solids bounded by a flat base and a height-field surface defined along a direction orthogonal to, and located strictly above, this base. For fabrication purposes the resulting blocks are required to cover the outer surface of input model, but are not required to cover its entire volume. We propose the first algorithm to partition a general 3D shape into a set of height-field blocks, leaving an axis aligned void inside.

The most significant application of height-field block decomposition is 3-axis CNC milling (Figure 1). In its most common and easiest to automate setting, automatic single-pass 3-axis CNC machining is limited to fabricating height-field blocks whose base is placed on the machining tray and whose axis is orthogonal to this tray (see further discussion in Sections 2, 6). CNC machining methods can be used to carve shapes from non-layerable materials such as wood or stone. They operate across a much wider range of scales and provide higher accuracy than 3D printing. Our decomposition algorithm allows fabrication of general 3D shapes using this methodology.
Height-block decomposition can also benefit fabrication techniques such as 3D printing, which requires supports when printing models with large overhangs. Eliminating supports reduces printing time and increases surface quality [Hu et al. 2014]. Decomposing a model into height-field blocks and printing these blocks separately allows for support-free 3D printing. Note that both applications only require the resulting blocks to cover the surface of the input model, and can often benefit from a decomposition that results in an interior voids due to obtained material savings.

**Problem Statement.** A height-field block decomposition of an input mesh should assign each point on the surface to a corresponding height-field block, covering the input surface. Blocks should never overlap and should remain strictly inside the input surface (see inset).

Additionally, to reduce manufacturing time and to facilitate easy assembly the number of blocks should be small and tiny blocks should be avoided. Based on these requirements, our algorithm’s goal can be formulated as computing a decomposition that satisfies the constraints above while simultaneously minimizing the number of blocks and maximizing the size of the smallest block. While this specific problem setting has not been investigated before, closely related problems such as minimal pyramidal decomposition, or covering a volume by non-overlapping height-field blocks [Hu et al. 2014; Fekete and Mitchell 2001], have been shown to be NP-hard and have no known exact or approximate polynomial time solutions. To obtain a pyramidal decomposition within an acceptable computation time Hu et al. [2014] significantly relax the height-field constraints and consider only a finite set of possible height-field orientations. In our setting such unbounded relaxation is not possible, since the identified constraints are critical for manufacturing. Our major observation is that we can always guarantee a valid solution by restricting the set of possible block base and side face orientations to the major axis directions. We use this observation to develop an algorithm that is guaranteed to obtain valid decompositions that satisfy the height-field constraints exactly or up to a specified tolerance and can be computed within a feasible time frame. As shown by our results, our algorithm robustly produces decompositions with acceptable, even if sub-optimal, block counts for a range of complex geometries. Our framework supports additional fabrication-motivated constraints: users can limit block sizes to ensure that each block fits into the machining chamber, or limit block height to reduce local thickness and introduce inner cavities to save material (Figure 6).

**Contribution.** Our core contribution is a computational solution to both exact and controlled height-field decomposition. We demonstrate the practical applicability of our algorithm on 5 fabricated results, four milled (Figures 1 and 12) and one 3D printed (Figure 14), and compare our method against potential alternatives (Figures 3 and 15). To ensure replicability of our results and to accelerate adoption of our technique, we provide a reference open-source implementation of our algorithm in the supplemental material.

## 2 RELATED WORK

Our work fits into the highly active domain of geometry processing for digital fabrication [Livesu et al. 2017; Medeiros e Sá et al. 2016]. Many of these techniques require decomposing models prior fabrication based on different criteria. We complement these methods by providing a new decomposition technique that strictly satisfies constraints that arise in contexts such as 3-axis CNC milling and overhang-free printing. Below we review the related decomposition technologies.

**Surface Segmentation.** Numerous method had been proposed for segmenting a surface model into charts that meet some prescribed requirement [Shamir 2008]. The general frameworks they employ are focused on surface features, and do not consider volumetric constraints. While they can potentially be modified to use height-field approximation as a desired chart property, they allow for no obvious extension to address our volumetric constraints such as block overlap avoidance.

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*Fig. 2. From height-field segmentations to height-field solid blocks: (a) two alternative height-field segmentations defined on the boundary of a simple shape. Top one uses arbitrary directions, the bottom is constrained to the global axes; (b) the resulting minimal solid blocks with flat base defined by each height-field segment. Note that raising any of the bases would leave a portion of the boundary uncovered; (c) some blocks overlap in the interior of the shape (red extent); (d) overlaps are resolved by splitting the blocks along their supporting lines, thus increasing the number of blocks; (e) the split operation produces 4 invalid blocks out of 5 for the non axis aligned case (top right, red ovals). Inner blocks, in grey, are ignored as they are not strictly necessary to reproduce the input boundary. Constraining the height-field directions to the global axes we can always guarantee a valid solution (proof in Appendix B)*

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Complex with up and down pointing normals. Unfortunately, computing a
block. Thus neither method is suitable for our needs as we require
separating these parts along the equator may result in non-height-field
sections. Approximate volumetric convex decomposition methods exist [Kraevoy
et al. 2007], they do not produce a convex volume decomposition, as
they do not prevent the convex hulls of the computed charts from
overlapping, and do not prevent the height-field blocks induced by
the charts from intersecting. Approximate volumetric convex de-
composition, e.g. [Attene et al. 2008; Lien and Amato 2007], relaxes
the convexity requirements to obtain a smaller number of parts; sepa-
rating these parts along the equator may result in non-height-field
blocks. Thus neither method is suitable for our needs as we require
strict height-field constraint enforcement. Pyramidal decomposition
aims to decompose an entire volume into height-field blocks, or
pyramids. Fekete and Mitchell [2001] proved that both the 3D ver-
sion of this problem and the 2D version on polygons with holes are
NP-hard. To the best of our knowledge no known exact polynomial
time solutions exist.

Height-Field Decomposition for Fabrication. A number of papers
specifically address height-field decomposition for fabrication.
Alemanno et al. [2014] propose a user assisted method for decomposing 3D shapes into height-
field blocks. Their method is driven by a manually crafted inner structure, which describes the bases
and the orientations of each block, fully defining the block decomposition. Overlaps between pairs
of blocks, are resolved using an interlocking zipper pattern, where regions shared by multiple blocks are expected to satisfy the height-
field requirement for both blocks. This assumption does not hold
unless special care is taken in the construction of the inner base
structure (see inset). Our approach algorithmically computes the
inner structure and automatically resolves such configurations if
and when they occur (Section 4.3).

Hu et al. [2014] propose an algorithm for approximate pyrami-
dal decomposition and advocate using it for 3D printing. As they
observe, a height-field block (or pyramid) can be printed standing
on its base, thus maximizing its stability and ensuring that no sup-
port structures are needed to sustain it during fabrication. Since,
as observed earlier, exact pyramidal decomposition is NP-hard to
compute, they opt for only weak enforcement of height-field con-
strains and have no direct control on how far the results deviate
from a desired approximation accuracy (Figure 15). The method is
therefore unsuited for settings, such as 3-axis milling, where the
height-field constraint needs to be strictly satisfied. Our algorithm
can enforce both strict and fixed accuracy height-field constraints
(Section 5).

Herholz et al. [2015] decompose free-form shapes into a set of
approximate height-field surface charts for milling and molding.
Candidate height-field directions are sampled from the Gaussian
sphere with a saliency-based approach. As-rigid-as-possible defor-
mation is used to enforce the height-field condition on the charts
when violated. The method produces segmentations that induce
overlapping height-field blocks (Figure 3). In their milling examples
the authors resort to a manual process to hollow-out the back sides
of each part to produce overlap-free shell parts. By using height-field
blocks we remove the need for such manual backside processing
and guarantee overlap avoidance.

Gao et al. [2015] propose a multi-directional 3D printing system
that allows to fabricate an object around a cuboidal shell, using its six
facets as printing beds. The method is only suitable for genus zero
objects which can be segmented into six axis aligned approximate
height-field blocks. While the algorithm seeks for a solution that
minimizes the overhang angle it cannot guarantee that the resulting
angles will be below any specific threshold. Our framework can
provide both strictly height-field blocks and blocks with strictly
constrained overhang angles regardless of topology (Figures 14, 13).
We jointly refer to our first four constraints as block-fabrication constraints. They define the properties each individual block should satisfy. The block size can be further restricted along the height-field axis, as the block’s height affects the amount of material used, and reducing it shortens fabrication time and saves costs. The coverage and non-overlap conditions are necessary to assemble the target model from these blocks. We refer to a block decomposition which satisfies all six conditions as valid. The last criterion, while not mandatory, is important for real-life fabrication since an excessive number of blocks would make assembly too cumbersome to attempt, and thin features make the blocks fragile.

Algorithm. To obtain the desired decomposition we need to solve a highly constrained discrete-continuous optimization problem over a very large search space, the variables of which are: the number of blocks, the direction associated with each block, and the location and geometry of their bases. The key observation behind our framework is that if we initialize our height-field blocks via intersections of the input model with axis aligned boxes, then we can always produce a valid decomposition via a finite set of boolean operations (proof in Appendix B). Specifically, given such a set of blocks that jointly cover the input surface, we can split them along the planes of their bounding boxes (Figure 2, bottom). This splitting process allows for trivial overlap elimination via duplicated block removal. The resulting set of sub-blocks satisfies all our requirements. In particular, each sub-block is an intersection of a rectangular box with a section of the input surface a priori constrained to be a height-field, i.e. a height-field block. Note that using the same process on non-axis aligned blocks would not produce the desired result (Figure 2, top).

This hypothetical splitting process provides a robust height-field decomposition of the input, but will clearly generate a large number of blocks. In practice, rather than performing all such splits at once, we perform a more restricted set of Boolean operations that use a subset of the box bounding planes, and seek to minimize the number of blocks produced. Our process preserves the height-field property of each individual block and terminates once all overlaps are removed. Thus, in the worst case it produces the same block set as the basic splitting algorithm, but in practice its outputs are drastically more compact.

We initialize and constrain the height-blocks to be inside the model by using a volume-aware block growth process. We first compute a dense set of maximal size valid height-field blocks that jointly cover the surface of the input model without intersecting it (Figure 4b). We avoid redundant and costly intersection tests by reformulating the computation of each block as an unconstrained continuous optimization problem that we efficiently solve. We extract from this set a minimal subset that covers the entire input surface while keeping the overlaps between the selected blocks small (Figure 4c). Given this compact set of blocks, we perform a sequence of Boolean operations that remove all overlaps and jointly ensure that the resulting blocks retain the height-field property and can be assembled to form the desired output (Section 4.3). In computing the sequence we seek to minimize the number of blocks produced and to maximize the smallest feature size as much as possible, to avoid the creation of fragile components that might break during fabrication. The combined algorithm strictly enforces all manufacturing constraints, while producing decompositions into small number of blocks and preserving the input surface geometry.

4 METHOD

4.1 Initialization

The orientation of the input may impact the height-field block decomposition. We fix this degree of freedom by maximizing the alignment between the surface normals and the global axes, that is computing the rotation matrix $R$ that minimizes:

$$\arg\min_R \frac{\sum_{f \in F} A_f \| R(n_f) \|_1}{\sum_{f \in F} A_f},$$

with $n_f$ denoting face normals, and $A_f$ face areas. Similarly to [Gao et al. 2015], we solve this problem with a RANSAC approach, sampling the Gauss sphere with spherical Fibonacci and selecting the orientation that performs best. Although not optimal (Section 6), this initialization significantly impacts the final results. Across all the models shown in the paper, when compared with a random initialization, obtaining up to 8 times less blocks.
4.2 Partition into Overlapping Height-Field Blocks

The goal of this stage is to compute a set of individually valid height-field blocks that jointly cover the input surface, where each block is constrained to be an intersection of the input model and an axis aligned rectangular box. To produce a compact final decomposition we seek to minimize the number of blocks in this covering set. A greedy approach to generating such a set would be to start from a seed block, maximally grow it until it cannot be further extended without violating our constraints, and then add more blocks using a similar process until coverage is achieved. This approach is heavily dependent on the strategy used to compute seed blocks, and can result in drastically larger numbers of blocks than necessary. Instead, we use a more conservative, if more time consuming, strategy where we first compute a large set of maximal blocks that cannot be further extended without violating our block-fabrication constraints, and then select a minimal subset of them that satisfies our coverage constraint. We avoid time-consuming brute-force evaluation of fabrication constraints by precomputing valid solution spaces for block extension and constraining block computation to these spaces. This two stages process provides a suitable starting point for our overlap resolution system (Figure 4b). An advantage of this approach is that the initial maximal blocks can be computed entirely in parallel, allowing for a trivial speedup. While other strategies could be used to grow the initial maximal blocks, we found our solution to be simple to implement and robust.

4.2.1 Maximal Height-Field Block Set. We desire a set of maximal size axis aligned bounding boxes that provide a good starting point for selecting a compact subset that covers the entire model.

Problem Setting. The input to this stage is a closed, intersection-free, triangle mesh $S = (V, F)$, where $V$ is the set of its vertices and $F$ the set of faces. The output of this stage is a set $B$ of axis aligned boxes, where the geometry of each $b \in B$ is encoded via the positions of its extrema corners (ones with the smallest and largest coordinate values). A box $b$ is valid if its intersection with the input shape is a valid height-field block. We note that for closed volumes, this requirement can be recast as requiring the angle between the outward pointing normal of any input shape triangle fully or partially inside the box and the milling direction associated with the block to be acute. Evaluating this condition explicitly and repeatedly during maximal box computation can be prohibitively expensive. Below we describe an efficient way to sidestep such explicit evaluations.

Initialization. To ensure complete coverage, we initialize the set $B$ with the bounding boxes of all the mesh triangles. Since each triangle can be part of at most three outward oriented height-field surfaces, we create seed bounding boxes associated with only these three orientations. In general normal directions on a surface change gradually, thus we expect each of these boxes to be valid, i.e. only overlap triangles which satisfy the acute angle constraint vis a vis our three initial axis directions. Section 4.5 discusses a pre-process which can be applied to the models to enforce this condition, if not satisfied a priori.

Expansion. We seek to maximize the coverage provided by each box while satisfying validity conditions. The validity testing can be reduced to two conditions. First, and most important, we need to test whether the expanded box overlaps with any triangles whose normals point in the opposite direction to the box’s axis. Second, we must at all times ensure that the dimensions of the box does not exceed the dimensions of the milling machine processing volume. A naive approach to block computation would be to grow each box using small steps, e.g. adding one triangle at a time, terminating growth if and when the validity constraints are violated. However, the first test in particular can be quite time consuming, and repeatedly performing it for each box at each expansion step can be prohibitively computationally expensive for large models. Instead of testing constraints directly, we define a valid solution space for box expansion and constrain our maximization problem to this space. The solution spaces are defined independently for each of our six orientations and are reused for all blocks which share this orientation. They are formulated so as to simultaneously prevent constraint violation and enable easy continuous optimization of coverage maximization.
The energy of a box is then defined as the integral of the scalar field over all cells of the box, which can be represented as the sum of the integrals over all cells of the regular grid that intersect the box. Each one of these integrals represents a continuous value within each cell by using tricubic interpolation. In case of conflicts (i.e., grid vertices having incident cells containing both obtuse and acute angles with the milling direction) we break ties by considering the lowest value we obtained. We assign continuous values within each cell by using tricubic interpolation. The energy of a box is then defined as the integral of the scalar field over all cells of the box:

\[ E(b) = \iiint_b s \, dV \]

which can be represented as the sum of the integrals over all cells of the regular grid that intersect the box. Each one of these integrals can be evaluated in closed form; we provide the derivation of this integral and of its derivatives in Appendix A. Note that any box \( b \) with \( E(b) \neq \infty \) by construction satisfies our block-fabrication constants, with the exception of maximal size which is discussed in the next paragraph.

**Optimization.** We simultaneously grow all boxes to cover as much of the input surface as possible, while still keeping them valid. The boxes are expanded by minimizing \( E \), subject to additional hard constraints that limit the size of the boxes to prevent them from growing beyond our maximal size threshold, and constrain the initial seed triangle associated with each box to remain inside this box. Both sets of constraints can be expressed as linear inequalities with respect to the position and dimension of the box \( Cb \leq d \), leading to the following non-linear optimization with linear inequality constraints:

\[
\begin{align*}
\text{arg min}_b & \ E(b) \\
\text{s.t.} & \ Cb \leq d
\end{align*}
\]

We convert this constrained optimization into an unconstrained one using logarithmic barriers, and minimize it using BFGS with bisection line search. The optimization is stopped when the energy at the current iteration is smaller than \( \infty \) and its difference to the energy at the previous iteration is smaller than \( 10^{-6} \).

**Heuristic Pruning.** The collection of maximal height blocks extracted using this basic procedure is highly redundant. To improve performance we reduce the set of processed boxes as follows. First, instead of considering all three valid directions for each seed triangle, we only use the milling direction closest to its normal. Second, we seed (and grow) boxes at random triangles, evenly distributed over the surface, and stop seeding new boxes as soon as the entire surface is completely covered, i.e. as soon as all the triangles of the surface have been assigned to at least one height block. While this heuristic could in theory lead to inferior results, they work well in practice, as we demonstrate in Figure 6 (bottom part), where we compare the results obtained with and without pruning. The difference in quality is negligible, but the heuristics reduce the computation cost from 47 to 2 minutes.

### 4.2.2 Minimal Covering

After maximally expanding all block boxes, we compute a minimal subset of them which entirely covers the surface. Computing such a set amounts to solving the classical minimal set cover problem, known to be NP-complete [Cormen et al. 2001]. We obtain a solution by casting it as an integer linear programming problem:

\[
\begin{align*}
\text{arg min}_{\mathbf{x}} & \ 1^T \mathbf{x} \\
\text{s.t.} & \ \sum_i x_i a_i \geq 1 \\
& \ x_i \in \{0, 1\}
\end{align*}
\]

where \( x_i \) is the \( i \)-th entry of \( \mathbf{x} \), a vector of binary variables that indicates if the box \( a_i \) is kept in the minimal covering, \( a_i \) is a binary vector with as many entries as the faces of the input, and where a value of 1 indicates that the corresponding face is contained in the box. We use an off-the-shelf solver (http://www.gurobi.com/) to obtain a solution. While in theory the runtime for this step can be exponential, in practice the solver converges to a solution in minutes (Table 1).
4.3 Overlap Resolution

Given the set of height-field blocks produced by the minimal covering, we seek to resolve the overlaps between them with a minimal increase in the number of blocks and without introducing thin fragile features.

Single Pair. Before addressing the general case, we consider overlap resolution on an individual pair of blocks $b_1$ and $b_2$ (Figure 7). The overlap between the blocks can always be eliminated by subtracting one block from another, e.g., $b_2$ from $b_1$. In all but some special cases, which we will discuss later, such a subtraction keeps the number of blocks constant. Post-subtraction, the block $b_1 \setminus b_2$ may no longer satisfy the validity constraints (Figure 7a). Depending on the configuration, reversing the order and computing $b_2 \setminus b_1$ may result in two valid blocks, but it is not guaranteed. In many instances, no order can produce a valid result (Figure 7c). Invalid blocks created by subtraction have multiple bases - i.e., polygons orthogonal to the milling direction. Each such block $b_j \setminus b_i$ can be therefore converted into a set of valid blocks by splitting it along one or more of the planes it shares with block $b_j$, such that each such base defines a separate block. While this solution is guaranteed to work, we want to minimize the number of such splitting operations. The basic overlap resolution method for two blocks $b_1$ and $b_2$ can be hence formulated as follows: (1) if only one of the two differences is valid use this difference to form a solution (Figure 7a); (2) if both $b_1 \setminus b_2$ and $b_2 \setminus b_1$ are valid blocks, perform the subtraction operation that maximizes the smallest output block (Figure 7b); (3) otherwise, split one of the difference blocks to obtain valid sub-blocks, selecting the refinement that maximizes the smallest output block (Figure 7c).

Multi-Block. We extend this framework to the multi-block scenario by casting overlap resolution as finding a sequence of subtraction operations that minimizes the number of splits required to ensure output validity. When splitting is unavoidable, we prioritize split operations that avoid producing very small blocks.

We represent the relation between adjacent height-field blocks using a directed graph whose vertices represent blocks; each graph edge represents a subtraction order dependency between its end vertices. More formally, we introduce an edge from $b_j$ to $b_i$ if and only if the difference $b_j \setminus b_i$ is not a valid height block. Note that it is possible to have two opposite edges connecting the same pair of vertices if both subtraction orders produce invalid blocks (Figure 7c).

Cycles in this graph exactly correspond to scenarios where splitting cannot be avoided. To obtain the desired subtraction order, if the initial graph contains cycles, we first transform it into a directed acyclic graph (DAG) by breaking all the cycles (and splitting the associated blocks). We then produce a valid subtraction order by computing an optimal topological order on this acyclic graph. The overall complexity of this step is $O(|s|(n + e)(c + 1))$, where $|s|$ is the number of splits, $n$ is the number of vertices, $e$ is the number of edges, and $c$ is the number of cycles.

Reduction to a DAG. To break cycles in the graph we iteratively select an edge $b_1 \rightarrow b_2$ on each cycle and split $b_2 \setminus b_1$ along the height-field direction of $b_2$, generating two or more non-overlapping valid blocks. We are sure that they are valid relying on a simple assumption: cutting a block with any plane containing the milling direction keeps requirements Axis, Base, and Height-Field in both sub-blocks. The vertices corresponding to the generated sub-blocks, denoted $b_{2,1}, \ldots, b_{2,n}$, are then added to the graph. Note that each sub-block’s vertex can at most inherit the edges of its parent, excluding $b_1 \rightarrow b_2$ (since there is no intersection between $b_{2,1}$ and $b_{2,2}$ and neither of them intersects $b_1$). As a consequence, if the block $b_2$ participated in $n$ cycles, its sub-blocks can participate at most in $n − 1$ cycles. This observation guarantees that each refinement step reduces the total number of cycles that graph vertices participate in, and consequently ensures that the reduction process terminates in a finite number of steps, producing a DAG. We detect all the cycles in the graph using Johnson’s algorithm [Cormen et al. 2001]. Among all the edges participating in a loop, we give priority to the one that maximizes the size of the smallest height block created. The splitting algorithm stops when a DAG is obtained. Note that while it is guaranteed to succeed, this splitting strategy may produce sub-optimal height-field decompositions with more blocks than necessary (see Figure 8).

Topological Sorting. We produce a valid subtraction sequence by computing an optimal topological order on the resulting DAG. Producing a linear ordering of a DAG’s vertices such that for every directed edge $b_j \rightarrow b_i$, $b_j$ comes before $b_i$ is a classical problem in graph theory. Note that our directed edges encode pathological splitting orders, we therefore aim to find an inverse topological sorting of the DAG vertices (i.e., for every directed edge $b_j \rightarrow b_i$, $b_j$ should come before $b_i$). We pre-process the DAG by inverting the orientation of each directed edge (i.e., transforming the roots in leaves, and vice versa) and performing topological sorting. Among all the possible orderings, we favor the one that maximizes the size of the smallest height-field block. To do so, we use Kahn’s iterative algorithm [Kahn 1962], prioritizing the vertices associated with the smallest blocks. In short, the algorithm works as follows: at each
Fig. 7. Different block processing orders result in different decompositions: (a) independently on the processing order, two valid height blocks are produced; (b) processing the block $b_1$ before the block $b_2$ produces two valid height-fields, inverting the order one block is not a height-field; (c) no valid solution exists, independently on the processing order. In the latter case, splitting one of the boxes allows for a valid processing order.

Fig. 8. Our cycle splitting strategy may produce sub-optimal height-field decompositions containing more pieces than necessary. Left: a set of axis-aligned boxes jointly covering the surface. Middle: the resulting conflict graph encoding pathological subtraction orders. A loop is present, meaning that at least one box will be split to produce a DAG (Section 4.3). Right: a valid decomposition into four height-field blocks. This solution does not correspond to any box subtraction order, and therefore cannot be produced by our algorithm.

iteration we find the roots of the graph (vertices with no incoming edges — if the graph is a DAG at least one root always exists); we order them from the smallest to the biggest block, and use this order to perform the subtraction, removing their corresponding vertices from the DAG. We repeat the process, iteratively looking for new roots until all the vertices in the DAG have been processed (Figure 9). Note that the inverse of the resulting topological sorting can also be used to generate illustrated instructions that describe a valid assembly sequence, though we do not guarantee that a globally valid assembly sequence always exists (Section 6).

4.4 Improving Blocks Size and Shape
A shortcoming of the method described so far is that it does not explicitly prevent the generation of tiny blocks or blocks with narrow protruding features, which could potentially break during fabrication (due to the stress induced by the milling tip) or during assembly. Such features are usually generated when performing Boolean operations between blocks with close-by faces with similar orientation. We describe here a greedy twofold strategy that has no theoretical guarantees but that in our experiments successfully removes narrow features, leading to the formation of well shaped height blocks.

Block Snapping and Shrinking. We process the blocks selected by the minimal covering (Section 4.2.2), aiming to minimize the number of intersections between blocks before starting the overlap resolution (Section 4.3). First, we consider all pairs of face-adjacent blocks, that is blocks with same orientation faces for which the distance between these faces is less than a fixed amount (the default is one grid unit, the user can choose to change it). We sort all the candidate pairs according to these distances, and adjust their dimensions reducing the distance to zero, making them perfectly face-adjacent. We then consider the remaining set of intersecting blocks, and try to shrink them in order to avoid overlaps. Note that shrinking blocks may leave some portion of the surface uncovered, we therefore apply block shrinking if and only if complete surface covering is preserved. These steps result in a conflict graph with less arcs and typically less cycles, thus reducing the number of splits.
necessary to reduce it to a DAG. On average, using this strategy we decreased the number of box splits by 50%.

**Modified Processing Order.** If, by processing the blocks in the order computed in Section 4.3, we generate a tiny height-block or a narrow feature, we rollback the operation and modify the processing order, giving the current block higher priority w.r.t. all the blocks it overlaps (Figure 10). This maximizes the size of the sub-blocks derived from such height-block and typically the number of narrow features produced. We automatically detect small blocks by measuring their volume [Zhang and Chen 2001], and detect tiny features by measuring the distance between pairs of block side and base edges. More advanced approaches [Zhou et al. 2013] could be used instead but in our experiments this was not necessary since all the thin features were detected by the two criteria above.

**Post Processing.** The boolean processing may result in adjacent blocks with same height-field direction. To reduce block count we merge them into a single block, either by raising the base of the lower block along the height-field direction, or by lowering the base of the higher block. The condition for performing the first operation is that there are no surface triangles in between the old and the new base. The condition for performing the second operation is more complex: we need to make sure that the new block doesn’t intersect any other block in the decomposition, and that it still satisfies the height-field constraint. After moving one of the two bases, we merge the two blocks. This post-processing typically merges one or two pairs of blocks.

4.5 Faithfulness vs Complexity

Enforcing strict fabrication constraints on highly detailed models often results in an excessive number of height-field blocks. For practical applications, exact fidelity to the input can often be sacrificed to reduce block count and facilitate easier fabrication. We provide an optional mechanism that allows users to reduce reconstruction accuracy, or faithfulness, in exchange for a lower block count. We note that smoother, or less detailed, models typically require significantly fewer height-field blocks to reconstruct than their detailed counterparts. We consequently achieve our target using a two step procedure that removes high-frequency surface details before the decomposition, and reintroduces the removed details into each block subject to preserving the fabrication constraints (Figure 11). To remove high-frequency details from the input shape we use the low-pass filter proposed in [Taubin 1995]. After computing the height-field block decomposition we reintroduce the high-frequency details using a variation of the Laplacian surface reconstruction framework [Sorkine 2006], enriched with height-field constraints that ensure that the vertices assigned to each block remain above its base with respect to the milling direction and that no triangle flips its orientation. Specifically, after the block decomposition of the smooth geometry is computed, every vertex \( v_i \) is assigned to a block \( b_{v_i} \), which has a milling direction \( m_{v_i} \). We then reintroduce the details by minimizing the following energy:

\[
\arg\min_{v_i} \| \Delta v - \delta \|^2 \text{s.t.} \quad v_i \in b_{v_i}, \quad n_i(v) \cdot m_{v_i} \geq 0
\]

where \( \delta_i = \frac{1}{|N_i|} \sum_{v_j \in N_i} (v_i - v_j) \) are the differential coordinates of the original mesh [Sorkine 2006], and \( n_i \) is the normal of the triangle \( i \). Equation 7 ensures that every vertex is constrained to stay above the block’s base and can be modeled with a set of linear inequality constraints. Equation 8 prevents triangle normals from flipping and is a quadratic condition on the vertex positions. We minimize this energy using coordinate descent, by optimizing one vertex at a time and freezing the others. The per-vertex optimization is solved with Newton iterations and it typically converges within 5 iterations, recovering most of the details of the input meshes (Figure 11). Specifically, the average distance between the two models, measured with Metro [Cignoni et al. 1998], is less than \( 1 \times 10^{-4} \) times the bounding box diagonal.

 Initialization Constraints. Given an input mesh, we assume that bounding boxes of individual triangles define valid height blocks. This condition can be violated in two scenarios. In the first case the top or outer surface defined by the intersection of the box and the input model may not be a height-field. This situation can only occur on meshes with high-frequency features, and it is solved using our high-frequency removal preprocessing. Initial blocks can, in theory, intersect the input surface. This situation can only occur if the mesh triangle size is larger than the local feature size. Such situations can always be avoided by refining the mesh using one or more rounds of one-to-four triangle subdivision.

Fig. 11. To keep the number of height-field blocks low we trade faithfulness for complexity. Specifically, given a detailed model we run our method on a pre-filtered version with no high frequencies (left). We then maximally restore the details while preserving the height-field property everywhere (middle, right). This strategy allowed us to reduce the number of height-field blocks from 14 to 7.
5 RESULTS
Throughout the paper we demonstrate a range of models decomposed into height-field blocks using our approach, ranging from relatively simple (Spiky cube) to highly complex (Chinese lion, Lion vase) and from relatively smooth (Kitten) to highly detailed (Buddha, Bimba). All our output decompositions are fabrication ready and strictly satisfy all validity conditions. The number of blocks in our decompositions varies from single digits (Moai, Max Planck) to 63 for Fertility.

Milled Results. We milled four objects from solid blocks of two different woods: pinewood and beechwood; the former is softer and easier to mill while producing less detailed results, the latter is harder and needs a longer milling time but leads to more detailed models. We milled Moai (Figure 12) and MaxPlanck (Figure 1) from the pinewood blocks; Buddha and Egyptian Statue from the beechwood blocks (Figure 12). Moai was milled with a Roland Modela MDX40, while MaxPlanck, Buddha and Egyptian statue have been milled with a Stepcraft-2/840 Desktop CNC System. The milling paths have been automatically generated from our height block decompositions using Autodesk Fusion 360 (https://www.autodesk.com/products/fusion-360/overview). Moai is assembled from 12 blocks and is 27 centimeters tall; MaxPlanck from 8 blocks and is 22 centimeters tall; Buddha from 8 blocks and is 19 centimeters tall (we skipped the curved base since the model does not stay straight with it); the Egyptian Statue from 11 blocks and is 32 centimeters tall. They have been assembled using wood glue, as shown in the video sequences provided as additional material. After assembly, the seams on each model have been covered with...
wood putty and sanded with fine grain sandpaper. This procedure hides the seams, which are only visible in the discontinuities of the wood pattern. We tested an alternative procedure on Moai statuette: we covered it with water-based enamel and then polished it. The final appearance is shown in the inset.

**Height Control.** By controlling the maximal height of the produced blocks users can control the amount of material necessary to fabricate the object (Figure 6), trading material savings for increased block count.

**Internal Framework.** Restricting our milling directions to the six major axis does not only simplify the assembly of small models, where the large overlaps can be easily covered with glue or kept together using metal L-shaped connectors, but it also drastically simplifies the construction of large architectural-scale objects. In this scenario, the interior of the shape can be realized with a sup-

\[
\text{internal edges, and is kept together with a single type of joints:}
\]

\[
\text{since the height blocks are axis aligned, the only possible intersections of the beams are multiples of 90 degrees. The required joints are simple to fabricate and reusable. A virtual example for the Egyptian Statue is in the inset.}
\]

\[
\text{High-Frequency Models. While our method can directly generate brute-force decompositions for high-frequency inputs, such decomposition would inevitably lead to high block counts, due to the very restrictive fabrication constraints inherent in 3-axis CNC milling. Our optional high-frequency filtering algorithm (Section 4.5) leads to much simpler decompositions, while losing minimal surface details, as shown in Figure 11.}
\]

\[
\text{Comparison with [Hu et al. 2014]. As noted earlier, in contrast to our framework the method of Hu et. al [2014] has no direct control on how far its outputs deviate from the height-field or pyramidality constraints, and demonstrate results where these constraints are far from satisfied. To compare the two approaches, we repeat the experiment proposed in Figure 23 of [Hu et al. 2014] and show the results in Figure 15. Our method introduces less blocks to decompose the model, and, more importantly, our blocks are millable, while the}
\]

---

### Table 1. Model statistics: computation time (split into Maximal Height-Field Block Computation (MHFBC), Minimal Covering (MC), Overlap Resolution (OR), CSG Operations (B)); number of blocks; and the block height maximum used (as percentage of model diagonal, \(\infty\) means no height limit).

<table>
<thead>
<tr>
<th>Model</th>
<th>MHFBC</th>
<th>MC</th>
<th>OR</th>
<th>B</th>
<th># Blocks</th>
<th>Height</th>
</tr>
</thead>
<tbody>
<tr>
<td>Airplane</td>
<td>1&quot;41&quot;</td>
<td>1&quot;</td>
<td>1&quot;</td>
<td>9&quot;</td>
<td>11</td>
<td>(\infty)</td>
</tr>
<tr>
<td>Batman</td>
<td>33&quot;44&quot;</td>
<td>20&quot;</td>
<td>1&quot;</td>
<td>54&quot;</td>
<td>8</td>
<td>0.15</td>
</tr>
<tr>
<td>Bimba</td>
<td>25&quot;23&quot;</td>
<td>3&quot;</td>
<td>0.2&quot;</td>
<td>39&quot;</td>
<td>16</td>
<td>(\infty)</td>
</tr>
<tr>
<td>BU (orientation)</td>
<td>27&quot;40&quot;</td>
<td>9&quot;</td>
<td>2&quot;</td>
<td>27&quot;24&quot;</td>
<td>16</td>
<td>0</td>
</tr>
<tr>
<td>BU (no orientation)</td>
<td>27&quot;40&quot;</td>
<td>9&quot;</td>
<td>1&quot;</td>
<td>23&quot;</td>
<td>9</td>
<td>0</td>
</tr>
<tr>
<td>Buddha</td>
<td>61&quot;37&quot;</td>
<td>15&quot;</td>
<td>1&quot;</td>
<td>33&quot;</td>
<td>8 (7 milled)</td>
<td>0.125</td>
</tr>
<tr>
<td>Chinese Lion</td>
<td>7&quot;38&quot;</td>
<td>3&quot;</td>
<td>2&quot;</td>
<td>59&quot;</td>
<td>27</td>
<td>0.125</td>
</tr>
<tr>
<td></td>
<td>2&quot;35&quot;</td>
<td>14&quot;</td>
<td>0.1&quot;</td>
<td>6&quot;</td>
<td>2</td>
<td>(\infty)</td>
</tr>
<tr>
<td>Cube Spike</td>
<td>1&quot;19&quot;</td>
<td>4&quot;</td>
<td>0.1&quot;</td>
<td>9&quot;</td>
<td>6</td>
<td>0.4</td>
</tr>
<tr>
<td></td>
<td>47&quot;21&quot;</td>
<td>6&quot;48&quot;</td>
<td>0.1&quot;</td>
<td>13&quot;</td>
<td>6</td>
<td>0.4</td>
</tr>
<tr>
<td>David</td>
<td>26&quot;27&quot;</td>
<td>9&quot;</td>
<td>0.2&quot;</td>
<td>18&quot;</td>
<td>7</td>
<td>0.075</td>
</tr>
<tr>
<td>Dea</td>
<td>31&quot;33&quot;</td>
<td>20&quot;</td>
<td>0.2&quot;</td>
<td>21&quot;</td>
<td>7</td>
<td>0.075</td>
</tr>
<tr>
<td>Egea</td>
<td>15&quot;56&quot;</td>
<td>6&quot;</td>
<td>0.1&quot;</td>
<td>7&quot;</td>
<td>6</td>
<td>0.1</td>
</tr>
<tr>
<td>Egyptian Statue</td>
<td>16&quot;77&quot;</td>
<td>6&quot;</td>
<td>5&quot;</td>
<td>21&quot;</td>
<td>11</td>
<td>0.05</td>
</tr>
<tr>
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<td>39&quot;33&quot;</td>
<td>10&quot;</td>
<td>1&quot;</td>
<td>11&quot;</td>
<td>10</td>
<td>0.125</td>
</tr>
<tr>
<td>Fertility</td>
<td>15&quot;32&quot;</td>
<td>11&quot;</td>
<td>32&quot;</td>
<td>10&quot;20&quot;</td>
<td>63</td>
<td>(\infty)</td>
</tr>
<tr>
<td>Gentildonna</td>
<td>36&quot;23&quot;</td>
<td>9&quot;</td>
<td>0.1&quot;</td>
<td>20&quot;</td>
<td>10</td>
<td>0.125</td>
</tr>
<tr>
<td>Kitten</td>
<td>21&quot;25&quot;</td>
<td>6&quot;</td>
<td>2&quot;</td>
<td>59&quot;</td>
<td>25</td>
<td>0.05</td>
</tr>
<tr>
<td>Lincoln</td>
<td>8&quot;23&quot;</td>
<td>6&quot;</td>
<td>0.6&quot;</td>
<td>1&quot;41&quot;</td>
<td>14</td>
<td>0.125</td>
</tr>
<tr>
<td>Lion Vase</td>
<td>29&quot;24&quot;</td>
<td>8&quot;</td>
<td>0.4&quot;</td>
<td>14&quot;</td>
<td>10</td>
<td>0.175</td>
</tr>
<tr>
<td>Max Plank</td>
<td>15&quot;59&quot;</td>
<td>10&quot;</td>
<td>0.3&quot;</td>
<td>14&quot;</td>
<td>8</td>
<td>(\infty)</td>
</tr>
<tr>
<td>Mosai</td>
<td>12&quot;47&quot;</td>
<td>4&quot;</td>
<td>0.2&quot;</td>
<td>9&quot;</td>
<td>12</td>
<td>0.225</td>
</tr>
<tr>
<td>Pensatore</td>
<td>11&quot;4&quot;</td>
<td>9&quot;</td>
<td>0.1&quot;</td>
<td>29&quot;</td>
<td>7</td>
<td>0.1</td>
</tr>
</tbody>
</table>

\(\infty\) No pruning
Fig. 14. By relaxing the height-field constraint we can decompose an object into blocks whose top surface contains overhangs that are strictly smaller than a printer-specific threshold. Here we show an example of a decomposition with a maximal overhang of 30 degrees for the Lion Vase dataset (left, middle). Notice from the side view that the lion mouth contains a considerable amount of overhangs. Since the threshold we set is compatible with that of common FDM printers, we safely printed each block without using support structures, saving time and material, and achieving better surface quality (right).

outputs of Hu et al. do not satisfy the height-field property (highlighted with red ovals in Figure 15) and thus can only be fabricated with a 3D printer.

**3D Printing.** Our pipeline is designed to produce height-field blocks, but, with a minor modification, becomes a powerful tool to produce decompositions tailored for FDM 3D printers. These printers require support material to sustain overhanging parts with angles larger than 35–40 degrees. The support does not only increase printing time and wastes material [Vanek et al. 2014], but also lowers surface quality [Zhang et al. 2015]. Our method can be used to decompose an object into blocks whose top surface contains overhang that are strictly smaller than a printer-specific threshold by simply relaxing the height-field condition in Section 4.2.1, assigning an infinite value to the scalar field only when triangles have a larger overhang. We show an example of a decomposition with a maximal overhang of 30 degrees in Figure 14 (note that this is the only result with overhangs, all the other results are decomposed in height-field blocks).

**Implementation Details.** We implemented our algorithm in C++, using Eigen [Guennebaud et al. 2010] for linear algebra routines, Gurobi (http://www.gurobi.com) for branch and bound, and libigl for mesh booleans [Zhou et al. 2016; Jacobson et al. 2016]. We run all our experiments on a workstation with a 4-cores Intel i7-4790K processor clocked at 4.0 Ghz and 16 Gb of memory. Our method takes under one hour on even the most complex model (Buddha) with the runtime dominated by the initial maximal size block computation. A summary of the timings and number of height-field blocks for all our experiments is shown in Table 1 and we attach all our results (input/output) in obj format as additional material.

**6 CONCLUSIONS AND DISCUSSION**

We presented an automatic and robust pipeline to decompose a triangle mesh into a collection of non-overlapping, valid height-field blocks, which can be directly manufactured using a 3-axis CNC milling machine. Our method is compatible with existing milling systems, and can be used to produce high quality real-life replicas of complex virtual geometries in a range of sizes. Our pipeline is automatic and robust: the only hard requirement on the input is that it should be a closed surface. The number of blocks...
we produce is dependent on the input model complexity, and can significantly increase for models with narrow prominent features or high genus, resulting in objects that may be hard to assemble. Manual decomposition and independent processing of the different parts can help reduce the block count. Our output depends on the orientation of the model, which might lead to decompositions with more pieces than necessary. While our orientation choice works well for many models, manual orientation can sometimes reduce block count (Figure 16). While we explicitly seek to avoid blocks with small features and successfully avoid cases that lead to fabrication failures, we are not guaranteed to produce a decomposition with the smallest number of such blocks. We do not consider optimal cut placement, such as avoiding seams on salient features, as in [Herholz et al. 2015]. Preventing seam placement in certain regions could possibly be incorporated into our minimal covering step: boxes that only partially cover such regions can be discarded or have lower priority. Finally, while in our practical experience we had never encountered these problems, we provide no guarantees that internal voids introduced by our system do not affect balance or structural strength. An extensive FEM analysis should be performed, and possibly directly integrated in the form-finding.

Assemblability. Being a height-field, each block can be locally extracted with a linear motion parallel to its build direction [Attene 2015]. However, the extent of such motion may be limited by collisions with nearby blocks, thus preventing assemblability. We tested the existence of a valid assembly sequence only for the fabricated models in Figure 1 and 12. We do not guarantee the existence of a valid one for the other decompositions shown in the paper. In particular, for complex models such as the ones shown in Figure 13 a valid assembly sequence may not exist.

Height-Field Blocks and Milling. There are multiple milling machine configurations. Our algorithm produces height-field blocks that are face millable (i.e., no undercuts are allowed). Our height-field constraints can be relaxed for shoulder millable settings, where the drill bit can remove material sideways, generating some undercuts (for example to chamfer a hole) [Smid 2003]. The advantage of using the face milling configurations is the availability of off-the-shelf milling-path computation software that can perform the path computation automatically. We do not address all milling constraints, e.g., we do not account for drill-bit thickness, as these problems are complementary to our decomposition focus.
ACKNOWLEDGMENTS

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REFERENCES


A BOX-INTEGRATION OF A TRICUBIC SCALAR FIELD.

Let $B$ be an axis aligned box defined by its two extreme points $p = (p_x, p_y, p_z)$ and $q = (q_x, q_y, q_z)$ and $L$ a regular lattice. We define $S$ as the set of all the cubes $(s_{u,v,w})$ in the lattice $L$ partially or completely contained in $B$:

$$S : \{ s_{u,v,w} \in L | s_{u,v,w} \cap B \neq \emptyset \}$$

and we define $D$ as the set of triplets of indexes in $S$:

$$D : \{ (u,v,w) | s_{u,v,w} \in S \}$$

Each cube $s_{u,v,w}$ in $L$ is defined by its two extreme points $(x_m, y_m, z_p)$ and $(x_{m+1}, y_{m+1}, z_{p+1})$ and to each cube we associate a set of coefficients $a_{i,j,k}^{(u,v,w)}$ for performing the tricubic interpolation inside $s_{u,v,w}$. The interpolated value $f$ in a generic $(x, y, z)$ point inside $s_{u,v,w}$ is:

$$f(x, y, z) = \sum_{i=0}^{3} \sum_{j=0}^{3} \sum_{k=0}^{3} a_{i,j,k}^{(u,v,w)} x^i y^j z^k$$

The energy to minimize is given by the integral over $B$, hence the sum of all the integrals over the cubes inside $B$:

$$\min_{u,v,w \in D} \int_{x_{\min}}^{x_{\max}} \int_{y_{\min}}^{y_{\max}} \int_{z_{\min}}^{z_{\max}} f(x, y, z)$$

where:

$$x_{\min} = \begin{cases} x_m & \text{if } x_m > p_x \\ p_x & \text{otherwise} \end{cases} \quad x_{\max} = \begin{cases} x_{m+1} & \text{if } x_{m+1} < q_x \\ q_x & \text{otherwise} \end{cases}$$

and similarly for $y$ and $z$.

The parameters are the coordinates of the points defining $B$. To be sure that the starting box will always cover the first primitive, we sum to the energy a barrier function tending to $+\infty$ when one of the coordinates of $B$ is too near to one of the coordinates of the points to cover (i.e. the endpoints of a segment), and is 0 when the coordinates are enough far from these points as in [Schüller et al. 2013].

Suppose to have a set $C$ of points $c = (c_x, c_y, c_z)$ to be covered by our box $B$. For each $c \in C$ we will have a function for $p$ and for $q$:

$$\Phi_{c,t}(p_x) = \begin{cases} +\infty & \text{if } p_x \geq c_x \\ \frac{1}{g(p_x)} & \text{if } c_x - t < p_x < c_x \\ 0 & \text{if } p_x \leq c_x - t \end{cases}$$

$$\Phi_{c,t}(q_x) = \begin{cases} 0 & \text{if } q_x \geq c_x + t \\ \frac{1}{g(q_x)} & \text{if } c_x < q_x < c_x + t \\ +\infty & \text{if } q_x \leq c_x \end{cases}$$

and similarly for $y$ and $z$, where $t$ is $\frac{1}{2}$ of the lattice's edge, and $g$ is:

$$g(x) = \frac{1}{t^3} x^3 - \frac{3}{t^2} x^2 + \frac{3}{t} x$$

Defining

$$\Phi_{c,t}(p) = \Phi_{c,t}(p_x) + \Phi_{c,t}(p_y) + \Phi_{c,t}(p_z),$$

$$\Phi_{c,t}(q) = \Phi_{c,t}(q_x) + \Phi_{c,t}(q_y) + \Phi_{c,t}(q_z)$$

we can add the barriers to the energy function to minimize:

$$\min_{u,v,w \in D} \int_{x_{\min}}^{x_{\max}} \int_{y_{\min}}^{y_{\max}} \int_{z_{\min}}^{z_{\max}} f(x, y, z) + \sum_{c \in C} (\Phi_{c,t}(p) + \Phi_{c,t}(q))$$

B VALID HEIGHT-BLOCK DECOMPOSITION VIA AA BOX SPLITTING.

Let $B_1$ and $B_2$ be a pair of intersecting axis aligned height boxes associate to the milling directions $m_1$ and $m_2$, which are in the set $(\pm X, \pm Y, \pm Z)$. Since $B_1$ and $B_2$ are axis aligned, their intersection $B_I = B_1 \cap B_2$ is an axis aligned box. The planes on which the six facets of $B_I$ lie, partition both $B_1$ and $B_2$ into eight sub-boxes each, namely $B_{1,1}, \ldots, B_{1,8}$ and $B_{2,1}, \ldots, B_{2,8}$. Note that, since $B_1$ and $B_2$ intersect, there always exist two indices $i,j \in [1,8]$ such that $B_{1,i} \equiv B_{2,j} \equiv B_I$.

Let us now consider which milling directions, between $m_1$ and $m_2$, could be chosen for these sub-boxes. We can observe that: (i) $B_{1,1}$ and $B_{2,2}$ and all the sub-boxes are axis aligned, therefore the angle between the box facets and the milling direction is either $0^\circ$ or $90^\circ$; (ii) each sub-box of $B_1 (B_{1,1}, \ldots, B_{1,8})$ has $m_1$ as candidate milling direction, and each sub-box of $B_2 (B_{2,1}, \ldots, B_{2,8})$ has $m_2$ as candidate milling direction. The only exception is $B_I$, which has both $m_1$ and $m_2$ as candidate milling directions.

From (i) and (ii) descends that any sub-box has at least one valid milling direction with an axis aligned facet as supporting base. In other words a valid height block decomposition obtained by splitting the original boxes using axis aligned planes always exists. □

Note that this is true only for the special case of axis aligned boxes and milling directions; in any other case condition (i) would not be satisfied, as the angle between the box facets and the milling direction may be greater than $90^\circ$, thus violating the height-field condition.