

BOUNDARY CONDITIONS

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A. PONEV

Consider advection-diffusion equation with BC:

$$u_t + a u_x = d u_{xx}, \quad t > 0$$

$$0 < x < L = 1$$

$$\left\{ \begin{array}{l} u(0, t) = 1 \\ u(1, t) = 0 \end{array} \right. \quad \text{Dirichlet}$$

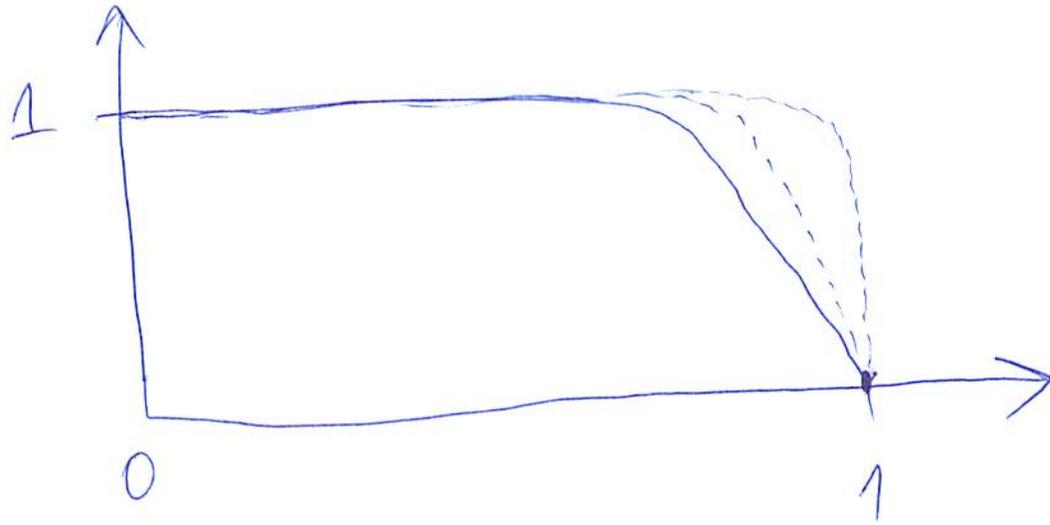
$$\left. \begin{array}{l} \text{or } \cancel{u} u_x(1, t) = 0 \quad \text{Neumann} \end{array} \right]$$

For Dirichlet, the steady-state

solution $u_t = 0 \Rightarrow a u_x = d u_{xx}$

$$u(x, t) = \frac{[e^{ax/d} - e^{ax/d}]}{[e^{a/d} - 1]}$$

②



Boundary layer of width $\sim d/a$

The solution forgets the boundary condition after a distance $\Delta x \sim d/a$ away from the boundary. \square

$$Pe = \left(\frac{\Delta x}{L} \right)^{-1} = \frac{aL}{d} \gg 1$$

this layer will be very thin!
(compare to AIR PLANE wing)

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If we used Neumann BC,

however, we would get

$$u(x, t) = 1$$

with no boundary layer.

This is what we often do in CFD if it is not important to resolve

the boundary layer: We make it disappear by using a fake

boundary condition (extrapolation from interior), as we will see

next.

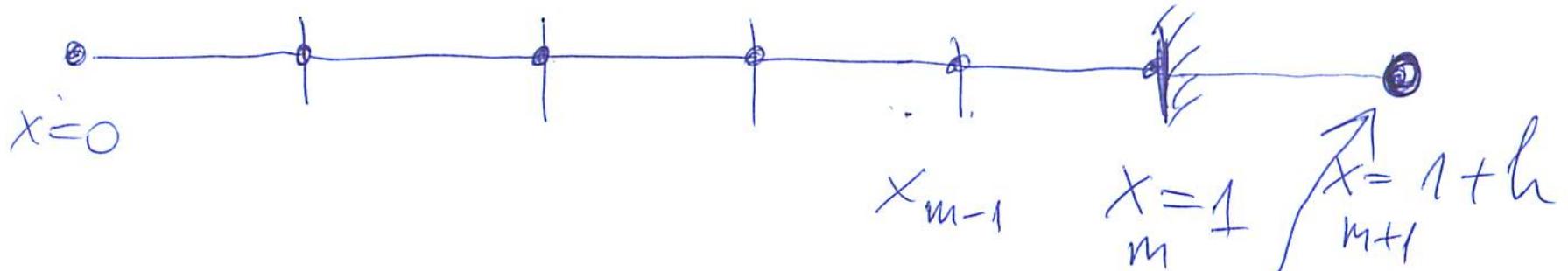
For now, assume smooth solution!

Consider first advection-dominated

(4)

flow:

$$\left\{ \begin{array}{l} u_t + u_x = 0, \quad x \in (0,1) \\ u(0,t) = g_0(t) \quad \text{inflow} \\ \text{no bc at outflow boundary} \end{array} \right.$$



Every CFD code has them!

"ghost" cell
or "virtual" cell

Assume we use centered difference
in the interior

centered difference

$$w_j' = \frac{1}{2h} (w_{j-1} - w_{j+1}) \quad (5)$$

At the left boundary,

$w_0(t) = f_0(t)$ follows from BC

At the right boundary, naive application of the same stencil leads to

$$w_m' = \frac{1}{2h} (w_{m-1} - w_{m+1})$$

But w_{m+1} is not a real variable.

Since there is no BC at right,

the best we can do is extrapolate from the interior

$$W_{m+1} = W_m - \text{constant extrapolation} \quad (6)$$

which leads to $w'_m = \frac{1}{2h} (W_{m-1} - W_m)$
or linear extrapolation

$$W_{m+1} = 2W_m - W_{m-1} \Rightarrow$$

$$W'_m = \frac{1}{2h} [W_{m-1} - 2W_m + W_{m-1}]$$

$$W'_m = \frac{1}{h} (W_{m-1} - W_m)$$

which ~~means~~ means we are using the
upwind scheme at the right boundary.
this makes sense!

So let us choose

$$w'_m = \frac{1}{h} (w_{m-1} - w_m)$$

(7)

which we can either implement in the code as a one-sided special stencil at the boundary, or, we can keep the same stencil but use a ghost cell $w_{m+1} = 2w_m - w_{m-1}$ (better?)

The problem we have now is that we switched from a second order to first order ~~local~~ local truncation error near the boundary.

spatial

We can prove that the scheme is still second-order accurate! (8)

Denote the local spatial truncation error with σ_h as before, and consider

$$w' = A w + g(t)$$

and assume that

$$\sigma_h = A \xi(t) + \eta(t)$$

Then, the global error

$$e' = A e + \sigma_h = A (e + \xi) + \eta$$

Take norms after variation of constants, exactly as before, to get

$$\tilde{e} = e + \xi$$

(9)

$$\tilde{e}' = A \tilde{e} + \xi'(t) + \eta(t)$$

$$\|e(t)\| \leq \|\xi\| + K e^{\omega t} \|e(0) + \xi(0)\| + \frac{K}{\omega} (e^{\omega t} - 1) \max_{0 \leq s \leq t} \|\xi'(s) + \eta(s)\|$$

This means that

Theorem: If $\|\xi\|, \|\xi'\|, \|\eta\| \leq C h^r$ $\forall t$

and $\|e(0)\| \leq C_0 h^r$, then

$$\|e(t)\| \leq \tilde{C}(t) h^r \leftarrow \begin{array}{l} \text{global order} = r \\ \text{local order} \end{array}$$

the difference with before is that (10)
this requires a bound on
 $\|\xi(t)\|$ and $\|\xi'(t)\|$ and $\|\eta(t)\|$

NOT on $\|\sigma_h(t)\|$. Recall

$$\sigma_h = A\xi + \eta \Rightarrow \xi \approx A^{-1}\sigma_h$$

Note that ξ_h is the solution of
the steady-state problem with

forcing $\boxed{g = \eta - \sigma_h}$. So the

local error acts as a source term
that then propagates through the global
solution, spatially.

Let's now go back to our (11)

example:

$$A = \frac{1}{2h} \begin{bmatrix} 0 & -1 & & & \\ 1 & & -1 & & \\ & 1 & & -1 & \\ & & \ddots & \ddots & \\ & & & 1 & 0 & -1 \\ & & & & \underline{2} & \underline{-2} \end{bmatrix} \leftarrow \text{boundary}$$

$$\begin{cases} \sigma_{h,m} = u_t(x_m, t) - \frac{1}{h} [u(x_{m-1}, t) - u(x_m, t)] \\ = -\frac{1}{2} h u_{xx}(x_m, t) + O(h^2) \end{cases}$$

Assume smoothness $\|u_{xx}\| \leq C_1$

$$\Rightarrow \begin{aligned} \sigma_{h,m} &\leq C_1 h \\ \sigma_{h,j < m} &\leq C_2 h^2 \end{aligned}$$

So we have

(12)

$$\sigma_h = \begin{bmatrix} 0 \\ \vdots \\ 0 \\ \vdots \\ 1 \end{bmatrix} c_1 h + \underbrace{O(h^2)}_{\eta}$$

and we need to solve

$$\sigma_h = A \xi + \eta \Rightarrow$$

$$\frac{1}{2h} \begin{bmatrix} 0 & -1 & \dots & 1 \\ \vdots & \vdots & \ddots & \vdots \\ 1 & \dots & \dots & 0 \\ \vdots & \vdots & \dots & \vdots \\ 2 & \dots & \dots & -2 \end{bmatrix} \xi = \begin{bmatrix} 0 \\ \vdots \\ 1 \end{bmatrix} c_1 h$$

This system we can solve by hand

$$\xi = [\dots, \xi_m, 0, \xi_m, 0, \xi_m]$$

where

$$\xi_m = C_1 h^2$$

note we gained!
one power

(13)

So indeed $\|\xi\| = O(h^2)$, $\|\eta\| = O(h^2)$

and the theorem tells us the

Spatial semi-discretization is

second-order accurate!

This is a very common occurrence, and we often do low-order discretizations near boundaries, even zeroth-order (!?)

(inconsistent) stencils next to boundaries.

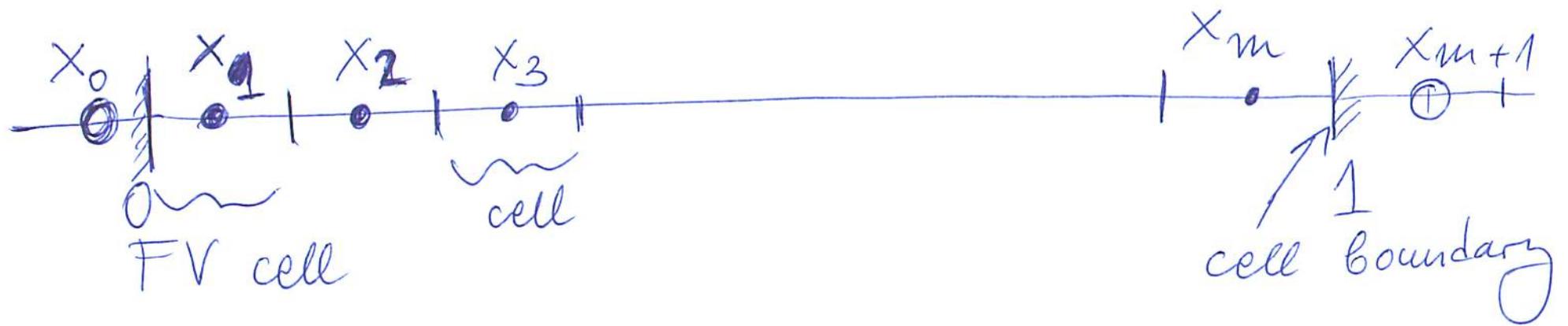
the hard part is stability

there is no simple ^{general} way to
analyze stability, i.e., to show $\textcircled{14}$
that $\|e^{tA}\| \leq K e^{wt}$ uniformly in h

The wisdom is that for schemes with
some (artificial or real) dissipation
stability is ensured by damping
instabilities near the
boundaries.
sufficient?

Often we rely on numerical experiments.
since instabilities are typically obvious.

For finite-volume schemes often (15)
 boundaries overlap with the faces
 of the grid, i.e., half-integer points in 1D:



$$x_j = \left(j - \frac{1}{2}\right) h, \quad h = 1/m$$

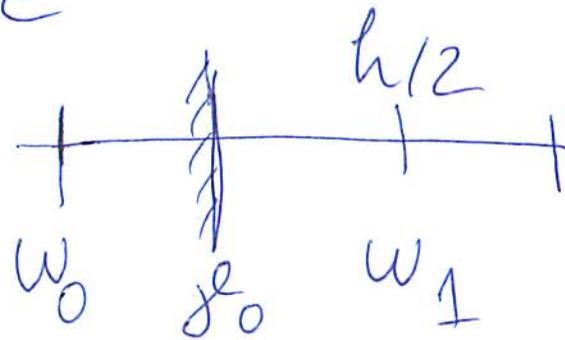
$$u_t = u_{xx} \quad \text{with BC} \quad \begin{cases} u(0, t) = g_0(t) \\ u_x(1, t) = g_1(t) \end{cases}$$

We need ghost values w_0 and w_{m+1}

Left: $\frac{w_0 + w_1}{2} = f_0$ ← linear
ext/interpolation
of BC

(16)

$$\Rightarrow \boxed{w_0 = 2f_0 - w_1}$$



Right: What Neumann BC really means
is no-flux through $x=1$:

$$F(x=1) = \frac{w_{m+1} - w_m}{\Delta x} = 0 \Rightarrow$$

$$\boxed{w_{m+1} = w_m}$$

(constant extrapolation)

Now consider advection - diffusion
with finite-volume

1

$$u_t + a u_x = d u_{xx}$$

Dirichlet BC gives flux directly
for advection, $f_{adv} = a u$

Neumann BC gives flux directly
for diffusion, $f_{diff} = -d u_x$

So for those fluxes we do not
need any interpolation/extrapolation
or ghost cells!

If we want our method to work for $d \rightarrow 0$ (pure advection) or advection-dominated flows, we must treat advection separately and realize that there is no BC at outflow for advection, only for diffusion.

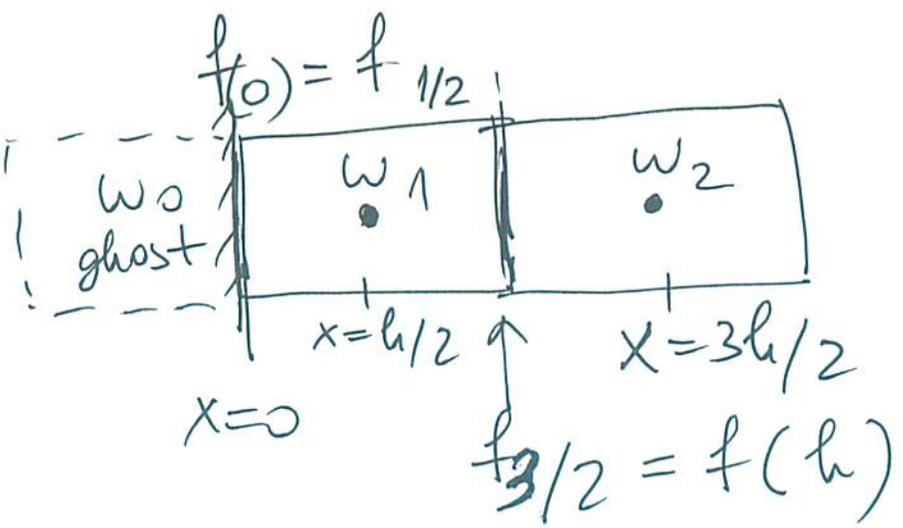
So treat diffusion as already explained in lecture notes

For advection, we need to consider second or third-order schemes separately.

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$$\left. \begin{aligned} u(0, t) &= \tilde{f}(t) \\ u_x(L, t) &= \tilde{g}(t) \end{aligned} \right\} \begin{array}{l} \text{Dirichlet on left} \\ \text{for diffusion but} \\ \text{does not matter for} \\ \text{advection!} \end{array}$$

At the right, we have outflow boundary
 and at the left, inflow boundary



$$f_{1/2} = f(0) = a \tilde{f}(t)$$

(flux at $x=0$)

$$f_{3/2} \approx f(x=h) = ?$$

An obvious choice is

① centered - advection:

$$f_{3/2} = -a \frac{w_1 + w_2}{2} \quad (\text{no ghost cell})$$

this gives (this is crucial to check)

$$\frac{dw_1}{dt} = -\frac{a}{h} (w_1 + w_2 - w_{1/2})$$

where $w_{1/2} \approx u(x=0) = \tilde{f}(t)$

A Taylor series expansion shows that this is first-order accurate at the boundary, which is ok since we get +1 order from $1/h$ in stencil.

NOTE: One can pretend here this is finite-difference

④*

At the outflow boundary, we want a one-sided stencil (no BC) so it is most natural to use first-order upwinding at outflow

(5*)

$$\frac{dw_N}{dt} = -\frac{a}{h} (w_N - w_{N-1})$$

Simple algebra shows that this is the same as using a ghost cell with linear extrapolation (MUST CHECK THIS!)

$$w_{N+1} = 2w_N - w_{N-1}$$