

Computational methods for suspensions of (cross-linked) slender fibers

Ondrej Maxian, Aleksandar Donev
Alex Mogilner, Brennan Sprinkle, Charles Peskin

Courant Institute, *New York University*

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Outline

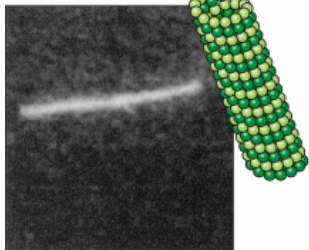
- 1 Motivation
- 2 Fibers in Stokes flow
 - Hydrodynamics
 - Adding twist
 - Inextensibility
- 3 Numerical Methods
- 4 Actin gels
- 5 Adding Brownian motion

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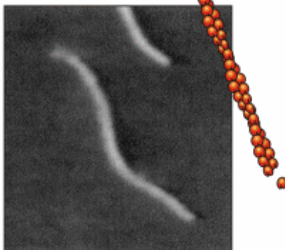
Fibers involved in cell mechanics

microtubules
 $\varnothing \approx 24 \text{ nm}$



stiff rods ($L_p \gg L$)

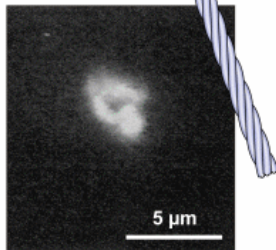
actin filaments
 $\varnothing \approx 7\text{-}9 \text{ nm}$



semiflexible ($L_p \approx L$)

Pawlizak and Käs, University of Leipzig

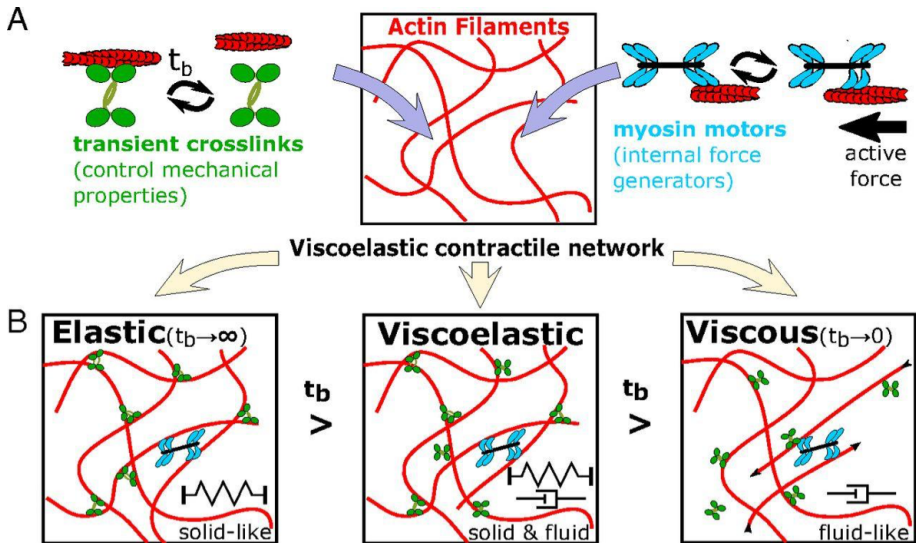
intermediate filaments
 $\varnothing \approx 10 \text{ nm}$



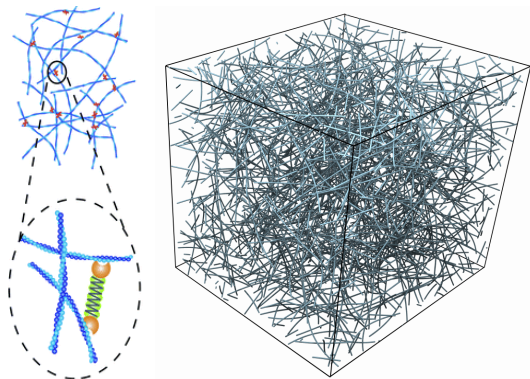
flexible ($L_p \ll L$)

L_p = persistence length, L = fiber length, $a = \epsilon L$ = fiber radius,
 ϵ = slenderness ratio

Cytoskeleton rheology

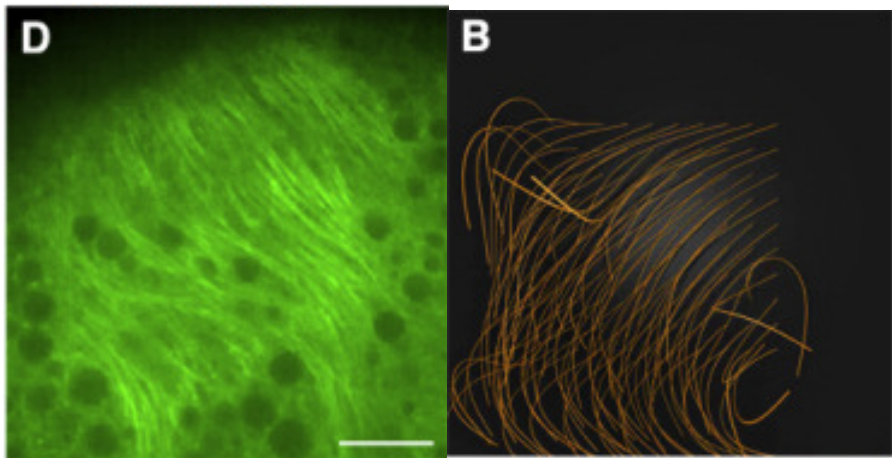
Ahmed and Betz. *PNAS*. (2015)

Cross-linked actin gels



- Very **slender semi-flexible fibers** (aspect ratio $10^2 - 10^4$) suspended in a **viscous solvent**.
- For now **cross linkers** modeled as simple elastic springs.
- **Periodic cyclically sheared** unit cell: **viscoelastic moduli**.

Does nonlocal hydrodynamics matter?



Monteith et al. Biophysics Journal. (2016)

Does nonlocal hydrodynamics matter?

- Sometimes flows created by individual fibers add up constructively to produce **large-scale flows**, which advect network.
- For example, cytoplasmic streaming on previous slide or contraction of a myosin-actin gel (must expel liquid out).
- Flow is generated at scales of fiber thickness: **multiscale problem**.
- Role of **long-ranged (nonlocal) hydrodynamics** unclear for rheology of cross-linked actin gels.

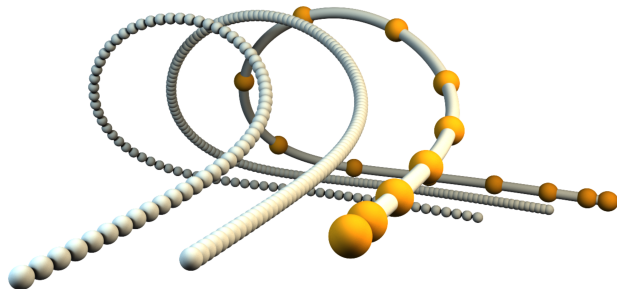
Dynamics of Flexible Fibers in Viscous Flows and Fluids, Ann. Rev. Fluid Mech. 51:539, du Roure, Lindner, Nazockdast, Shelley [1]

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Fiber Representation

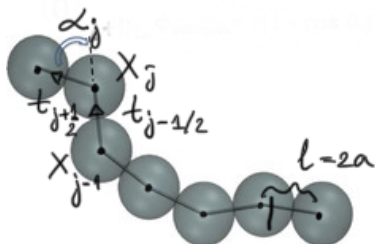
Simple approach is to represent a fiber as a **discrete chain** of beads/blobs: **multiblob model**



More efficient approach is to represent a fibers as **continuum curve**
O. Maxian et al. ArXiv:2201.04187

An integral-based spectral method for inextensible slender fibers in Stokes flow [2]
The hydrodynamics of a twisting, bending, inextensible fiber in Stokes flow [3]

Inextensible multilob chains



Worm-like polymer chain

- Inextensibility: $\|\mathbf{X}_{j+1} - \mathbf{X}_j\| = l \sim a$ (e.g., a or $2a$).
- Tangent vectors:

$$\boldsymbol{\tau}_{j+1/2} = (\mathbf{X}_{j+1} - \mathbf{X}_j) / l$$
- Bending angles:

$$\cos \alpha_j = \boldsymbol{\tau}_{j+1/2} \cdot \boldsymbol{\tau}_{j-1/2}$$
- Elastic energy (bending modulus κ_b)

$$E_b = \frac{2\kappa_b}{l} \sum_{j=1}^{N-1} \sin^2 \left(\frac{\alpha_j}{2} \right)$$

Inextensible continuum fibers

- Persistence length due to thermal fluctuations $\xi = 2\kappa_b / (k_B T) \gg l$ gives us a **continuum limit**, $\alpha_j \ll 1$.
- Fiber centerline $\mathbf{X}(s)$ where the **arc length** $0 \leq s \leq L$.
- The tangent vector is $\boldsymbol{\tau} = \partial\mathbf{X}/\partial s = \mathbf{X}_s$, and the **fibers are inextensible**,

$$\boldsymbol{\tau}(s, t) \cdot \boldsymbol{\tau}(s, t) = 1 \quad \forall (s, t).$$

- Bending energy functional is integral of curvature squared:

$$E_b(\mathbf{X}) = \frac{2\kappa_b}{l} \sum_{j=1}^{N-1} \left(\frac{\alpha_j}{2}\right)^2 \quad \Rightarrow \quad E_b[\mathbf{X}(\cdot)] = \frac{\kappa_b}{2} \int ds \|\mathbf{X}_{ss}(s)\|^2$$

Bending elasticity

- Bending force $\mathbf{F}_j^{(b)}$ on interior blob j gives us **elastic force density**

$$\mathbf{F}_j^{(b)} = -\frac{\partial E_b}{\partial \mathbf{X}_j} = \frac{\kappa_b}{l^3} (-\mathbf{X}_{j-2} + 4\mathbf{X}_{j-1} - 6\mathbf{X}_j + 4\mathbf{X}_{j+1} - \mathbf{X}_{j+2})$$

$$\mathbf{F}_b \approx -l\kappa_b \mathbf{D}^4 \mathbf{X} \quad \Rightarrow \quad \mathbf{f}_b = -\frac{\delta E_{\text{bend}}}{\delta \mathbf{X}} = -\kappa_b \mathbf{X}_{\text{ssss}}$$

- Endpoints naturally handled discretely, giving in continuum natural BCs for **free fibers**:

$$\mathbf{X}_{\text{ss}}(0/L) = 0, \quad \mathbf{X}_{\text{sss}}(0/L) = 0.$$

- Tensions** $T_{j+1/2} \rightarrow T(s)$ are **unknown** and resist stretching,

$$\Lambda_i = T_{i+1/2} \boldsymbol{\tau}_{i+1/2} - T_{i-1/2} \boldsymbol{\tau}_{i-1/2} \quad \Rightarrow \quad \boldsymbol{\lambda} = (T\boldsymbol{\tau})_s.$$

Fluid dynamics

- For multiblob chains in **Stokes flow**, fluid velocity $\mathbf{v}(\mathbf{r}, t)$ satisfies $\nabla \cdot \mathbf{v} = \mathbf{0}$ and

$$\nabla \pi = \eta \nabla^2 \mathbf{v} + \sum_j \mathbf{F}_j \delta_a(\mathbf{X}_j - \mathbf{r}),$$

where $\delta_a(\mathbf{r})$ is a **blob kernel** of width $\sim a$, and

$$\mathbf{F} = -l\kappa_b \mathbf{D}^4 \mathbf{X} + \Lambda$$

- Blobs/fiber are advected by fluid

$$\mathbf{U}_j = d\mathbf{X}_j/dt = \int d\mathbf{r} \mathbf{v}(\mathbf{r}, t) \delta_a(\mathbf{X}_j - \mathbf{r}).$$

- Continuum limit is obvious (without Brownian fluctuations)

$$\nabla \pi(\mathbf{r}, t) = \eta \nabla^2 \mathbf{v}(\mathbf{r}, t) + \int_0^L ds \mathbf{f}(s, t) \delta_a(\mathbf{X}(s, t) - \mathbf{r})$$

$$\mathbf{U}(s, t) = \partial_t \mathbf{X}(s, t) = \int d\mathbf{r} \mathbf{v}(\mathbf{r}, t) \delta_a(\mathbf{X}(s, t) - \mathbf{r})$$

$$\mathbf{f} = -\kappa_b \mathbf{X}_{ssss} + \lambda$$

Multiblob chains in Stokes flow

- We can (temporarily) eliminate the fluid velocity to write an equation for **fiber only**.
- Define the positive semi-definite **hydrodynamic kernel**

$$\mathcal{R}(\mathbf{r}_1, \mathbf{r}_2) = \int \delta_a(\mathbf{r}_1 - \mathbf{r}') \mathbb{G}(\mathbf{r}', \mathbf{r}'') \delta_a(\mathbf{r}_2 - \mathbf{r}'') d\mathbf{r}' d\mathbf{r}'',$$

where \mathbb{G} is the Green's function for (periodic) Stokes flow.

- Define $\mathbf{M}(\mathbf{X}) \succeq \mathbf{0}$ to be the symmetric positive semidefinite (SPD) **mobility matrix** with blocks

$$\mathbf{M}_{ij}(\mathbf{X}_i, \mathbf{X}_j) = \mathcal{R}(\mathbf{X}_i, \mathbf{X}_j) = \mathcal{R}(\mathbf{X}_i - \mathbf{X}_j).$$

- Discrete dynamics = **inextensibility** +

$$\mathbf{U} = d\mathbf{X}/dt = \mathbf{M}(\mathbf{X}) \mathbf{F}(\mathbf{X}) = \mathbf{M}(-l\kappa_b \mathbf{D}^4 \mathbf{X} + \mathbf{\Lambda})$$

Inextensible fibers in Stokes flow

- Define a positive semidefinite **mobility operator**

$$(\mathcal{M}[\mathbf{X}(\cdot)] \mathbf{f}(\cdot))(s) = \int_0^L ds' \mathcal{R}(\mathbf{X}(s), \mathbf{X}(s')) \mathbf{f}(s')$$

- Continuum dynamics is a **non-local PDE**

$$\mathbf{U} = \mathbf{X}_t = \mathcal{M}[\mathbf{X}] (-\kappa_b \mathbf{X}_{ssss} + \boldsymbol{\lambda})$$

$$\boldsymbol{\tau}(s, t) \cdot \boldsymbol{\tau}(s, t) = 1 \quad \forall (s, t).$$

- Is this PDE well-posed? We have shown *numerically* that
 - Fiber velocity converges pointwise (strongly) up to the endpoints.
 - Moments of $\boldsymbol{\lambda}$ converge**, e.g., stress tensor (weak convergence).

Rotne-Prager-Yamakawa kernel

$$\mathcal{R}(\mathbf{r}_1, \mathbf{r}_2) = \int \delta_a(\mathbf{r}_1 - \mathbf{r}') \mathbb{G}(\mathbf{r}', \mathbf{r}'') \delta_a(\mathbf{r}_2 - \mathbf{r}'') d\mathbf{r}' d\mathbf{r}''$$

- Taking the regularization kernel and unbounded Stokes flow

$$\delta_a(\mathbf{r}) = (4\pi a^2)^{-1} \delta(r - a)$$

gives the **Rotne-Prager-Yamakawa (RPY) kernel**

$$\mathcal{R}(\mathbf{r}) = \begin{cases} (8\pi\eta)^{-1} \left(\mathcal{S}(\mathbf{r}) + \frac{2a^2}{3} \mathcal{D}(\mathbf{r}) \right), & r > 2a \\ (6\pi a\eta)^{-1} \left[\left(1 - \frac{9r}{32a} \right) \mathbf{I} + \left(\frac{3r}{32a} \right) \frac{\mathbf{r} \otimes \mathbf{r}}{r^2} \right], & r \leq 2a \end{cases}$$

$$\mathcal{S}(\mathbf{r}) = \frac{1}{8\pi\eta r} \left(\mathbf{I} + \hat{\mathbf{r}}\hat{\mathbf{r}}^T \right) \equiv \mathbb{G}, \quad \text{and} \quad \mathcal{D}(\mathbf{r}) = \frac{1}{8\pi\eta r^3} \left(\mathbf{I} - \hat{\mathbf{r}}\hat{\mathbf{r}}^T \right)$$

Slender Body Theory

$$(\mathcal{M}[\mathbf{X}(\cdot)] \mathbf{f}(\cdot))(s) = \int_0^L ds' \mathcal{R}(\mathbf{X}(s) - \mathbf{X}(s')) \mathbf{f}(s')$$

- **Matched asymptotics** gives (away from endpoints)

$$\begin{aligned} (\mathcal{M} \mathbf{f})(s) &\approx (\mathcal{M}_{\text{SBT}} \mathbf{f})(s) = (\mathcal{M}_{\text{L}} \mathbf{f})(s) + (\mathcal{M}_{\text{NL}} \mathbf{f})(s) = \\ &= \frac{1}{8\pi\eta} \left(\log \left(\frac{(L-s)s}{4a^2} \right) (\mathbf{I} + \boldsymbol{\tau}(s)\boldsymbol{\tau}(s)^T) + 4\mathbf{I} \right) \mathbf{f}(s) \\ &\quad + \frac{1}{8\pi\eta} \int_0^L ds' \left(\boldsymbol{\mathcal{S}}(\mathbf{X}(s) - \mathbf{X}(s')) \mathbf{f}(s') - \left(\frac{\mathbf{I} + \boldsymbol{\tau}(s)\boldsymbol{\tau}(s)^T}{|s-s'|} \right) \mathbf{f}(s) \right) \end{aligned}$$

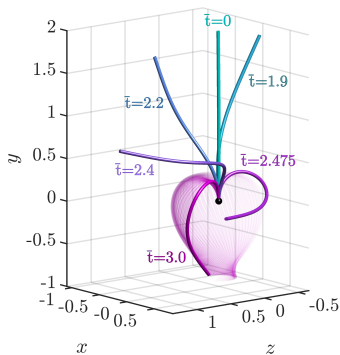
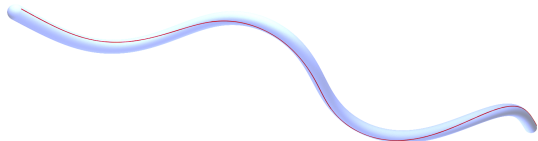
- For a special choice of blob radius $a = (e^{3/2}/4) \epsilon L = 1.12\epsilon L$, this formula matches the widely-used **Slender Body Theory** (SBT).
- Our approach automatically works for **multiple fibers**, and also gives us a natural **regularization of the endpoints** (not shown).

Slender body theory

$$\mathcal{M}_{\text{SBT}} = \mathcal{M}_{\text{L}} + \mathcal{M}_{\text{NL}} = \mathcal{O} \left(\log \left(\frac{(L-s)s}{a^2} \right) \right) + \mathcal{O}(1)$$

- SBT is great for numerics since it involves **quadratures** that can be computed accurately for smooth \mathbf{f} to **spectral accuracy** (starting with Tornberg+Shelley = TS).
- The local drag term is logarithmically **singular at endpoints** for cylindrical fibers.
TS use (unphysical) **ellipsoidal fibers**: $\mathcal{M}_{\text{L}} = \mathcal{O}(\log(L/a))$.
- \mathcal{M}_{L} has **spurious negative eigenvalues** for high spatial frequencies, so \mathcal{M}_{SBT} is **not SPD** and equations are definitely **not well-posed**.
TS use **artificial regularization**.

Twisting Fibers



- How to represent twist (Bishop frame)?
- Hydrodynamics with twist? (no slender-body theory exists)
- (When) does twist matter?
Flagella, formins twisting growing actin filaments, macroscopic chirality in cells, and ?

Twist

- For given force densities $\mathbf{f}(s, t)$ and **parallel torque** densities $n(s, t)$ along the fiber centerlines,

$$\nabla\pi = \eta\nabla^2\mathbf{v} + \int_0^L ds \left[\mathbf{f}(s) + n(s)\frac{\nabla}{2} \times \boldsymbol{\tau}(s) \right] \delta_a(\mathbf{X}(s) - \mathbf{r}),$$

$$\Omega^{\parallel}(s) = \boldsymbol{\tau}(s) \cdot \int d\mathbf{r} \frac{\nabla}{2} \times \mathbf{v}(\mathbf{r}, t) \delta_a(\mathbf{X}(s) - \mathbf{r})$$

- Should fiber exert **perpendicular torques** on the fluid?
Not for sufficiently slender fibers (ArXiv:2201.04187) [3].

Bishop frame

- To each point along the fiber we attach an orthonormal triad $\mathbf{B}(s) = [\boldsymbol{\tau}(s), \mathbf{a}(s), \mathbf{b}(s)]$ called the **Bishop frame**, which satisfies the *no-twist condition*:

$$\mathbf{a}_s \cdot \mathbf{b} = 0 \quad \Rightarrow \quad \partial_s \mathbf{a} = (\boldsymbol{\tau} \times \boldsymbol{\tau}_s) \times \mathbf{a}$$

- Configuration represented by **twist angle** $\theta(s)$ between the material frame of the fiber cross section and the Bishop cross section.
- Elastic force has bend-twist coupling (belt trick):

$$\mathbf{f} = -\kappa_b \mathbf{X}_{ssss} + \kappa_t (\theta_s (\boldsymbol{\tau} \times \boldsymbol{\tau}_s))_s + \boldsymbol{\lambda},$$

$$n = \kappa_t \theta_{ss}.$$

- Evolve **twist density** in time via

$$\partial_t \theta_s(s, t) = \partial_s \Omega^{\parallel} - (\boldsymbol{\Omega}^{\perp} \cdot \boldsymbol{\tau}_s).$$

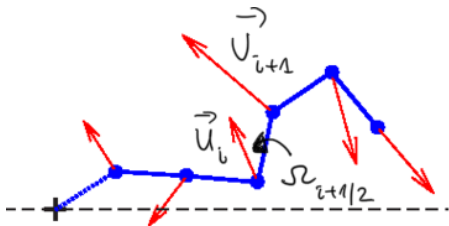
Tension equation

$$\mathbf{X}_t = \mathcal{M}[\mathbf{X}] (-\kappa_b \mathbf{X}_{ssss} + \boldsymbol{\lambda}) \quad \text{and} \quad \boldsymbol{\lambda} = (T\boldsymbol{\tau})_s$$

- Traditional approach (Tornberg+Shelley) is to solve **tension equation**

$$\boldsymbol{\tau} \cdot \boldsymbol{\tau} = \mathbf{X}_s \cdot \mathbf{X}_s = 1 \quad \Rightarrow \quad (\mathbf{X}_t)_s \cdot \mathbf{X}_s = 0 \quad \text{non-local BVP}$$
- Tension equation is linear in $T(s)$ but very nonlinear in \mathbf{X} and its derivatives, causing **aliasing issues**.
- Method does not strictly enforce inextensibility numerically, requiring adding a **penalty for stretching**.
- To solve these problems, let us first go back to multiblobs for simplicity, and then take a **continuum limit**.

Inextensible motions



$$\frac{\mathbf{U}_i - \mathbf{U}_{i-1}}{\Delta s} = \Omega_{j+1/2} \times \boldsymbol{\tau}_{j+1/2} \quad \Rightarrow$$

$$\mathbf{U} = \mathbf{K}\Omega^\perp = \left[\mathbf{U}_0, \dots, \mathbf{U}_0 + \Delta s \sum_{j=0}^{i-1} \Omega_{j+1/2}^\perp \times \boldsymbol{\tau}_{j+1/2}, \dots \right] \rightarrow$$

$$\left(\boldsymbol{\kappa}[\mathbf{X}(\cdot)] \Omega^\perp(\cdot) \right) (s) = \mathbf{U}(s) = \mathbf{U}(0) + \int_0^s ds' \left(\Omega^\perp(s') \times \boldsymbol{\tau}(s') \right).$$

Principle of virtual work

- **Principle of virtual work:** Constraint forces should do no work for any inextensible motion of the fiber:

$$\mathbf{\Lambda}^T \mathbf{U} = (\mathbf{K}^T \mathbf{\Lambda})^T \mathbf{\Omega}^\perp = 0 \quad \forall \mathbf{\Omega}^\perp \quad \Rightarrow \quad \mathbf{K}^T \mathbf{\Lambda} = \mathbf{0}$$

$$\mathbf{K}^T \mathbf{\Lambda} = \left[\sum_{j=0}^N \mathbf{\Lambda}_j, \dots, \Delta s \left(\sum_{j=i}^N \mathbf{\Lambda}_j \right) \times \boldsymbol{\tau}_{i+1/2}, \dots \right] \rightarrow$$

$$(\mathcal{K}^* [\mathbf{X}(\cdot)] \boldsymbol{\lambda}(\cdot))(s) = \left[\int_0^L ds' \boldsymbol{\lambda}(s'), \forall s \left(\int_s^L ds' \boldsymbol{\lambda}(s') \right) \times \boldsymbol{\tau}(s) \right] = 0.$$

- We can express this in terms of tension

$$\forall s \quad \int_s^L ds' \boldsymbol{\lambda}(s') = -T(s) \boldsymbol{\tau}(s) \quad \Rightarrow \quad \boldsymbol{\lambda} = (T \boldsymbol{\tau})_s$$

but the principle of virtual work is an **integral constraint**.

Continuum equations

- New **weak formulation of inextensibility** constraint:

$$\mathbf{X}_t = \mathcal{K}[\mathbf{X}] \Omega^\perp = \mathcal{M}[\mathbf{X}] (-\kappa_b \mathbf{X}_{ssss} + \lambda)$$

$$\mathcal{K}^*[\mathbf{X}] \lambda = \mathbf{0}$$

$$\partial_t \boldsymbol{\tau} = \Omega^\perp \times \boldsymbol{\tau}$$

$$\mathbf{X}(s, t) = \mathbf{X}(0, t) + \int_0^s ds' \boldsymbol{\tau}(ds', t)$$

- Two improvements:
 - Evolve tangent vector $\boldsymbol{\tau}$ rather than \mathbf{X} : **strictly inextensible**.
 - Expose **saddle-point structure** of problem (energy conservation).

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Slender-Body Quadrature

- Recall slender body *theory* (SBT) $\mathcal{M}_{\text{SBT}} = \mathcal{M}_{\text{L}} + \mathcal{M}_{\text{NL}}$.
- We avoid SBT via **slender body quadrature** for RPY

$$\mathbf{U}(s) = \int_{D(s):|s-s'|>2a} \left(\mathbb{S}(\mathbf{X}(s), \mathbf{X}(s')) + \frac{2a^2}{3} \mathbb{D}(\mathbf{X}(s), \mathbf{X}(s')) \right) \mathbf{f}(s') ds' \\ + \int_{s-2a}^{s+2a} (\dots \text{RPY} \dots) \mathbf{f}(s') ds'.$$

- Apply **singularity subtraction** even though not technically singular:

$$\int_{D(s)} \mathbb{S}(\mathbf{X}(s), \mathbf{X}(s')) \mathbf{f}(s') ds' = \frac{1}{8\pi\eta} \int_{D(s)} \left(\frac{\mathbf{I} + \boldsymbol{\tau}(s)\boldsymbol{\tau}(s)}{|s-s'|} \right) \mathbf{f}(s) ds' \\ + \int_{D(s)} \left(\mathbb{S}(\mathbf{X}(s), \mathbf{X}(s')) \mathbf{f}(s') - \frac{1}{8\pi\eta} \left(\frac{\mathbf{I} + \boldsymbol{\tau}(s)\boldsymbol{\tau}(s)}{|s-s'|} \right) \mathbf{f}(s) \right) ds'$$

- Taking the domain $D(s)$ to be $[0, L]$ in the second gives the finite part integral from SBT!

Spatial Discretization

- We develop a **spectral discretization** in space, based on representing all functions using **Chebyshev polynomials**, with **anti-aliasing**.
- **Collocation discretization** of mobility equation gives a **saddle-point system**

$$\begin{pmatrix} -\mathbf{M}(\mathbf{X}) & \mathbf{K}(\mathbf{X}) \\ \mathbf{K}^*(\mathbf{X}) & \mathbf{0} \end{pmatrix} \begin{pmatrix} \lambda \\ \Omega \end{pmatrix} = \begin{pmatrix} \mathbf{M}(\mathbf{X})(-\kappa_b \mathbf{D}_{BC}^4 \mathbf{X}) \\ \mathbf{0} \end{pmatrix}$$

which we solve iteratively using a **block-diagonal preconditioner**.

- We only use $O(16 - 32)$ Chebyshev points per fiber so doing **dense LA for individual fibers** is OK.
- Bending elasticity can either be discretized using **rectangular collocation** (more accurate, needs BCs) or by discretizing bending energy functional (more robust, **natural BCs**).

Temporal discretization

- **Backward Euler** is the most stable since it ensures strict energy dissipation; also for *dense* suspensions.
- **Split** mobility into **local** (e.g., intra-fiber) and **non-local** (e.g., inter-fiber) parts, $\mathbf{M} = \mathbf{M}_L + \mathbf{M}_{NL}$:

$$\begin{aligned} \mathbf{K}^n \boldsymbol{\Omega}^n &= \mathbf{M}_L^n \left(-\kappa_b \mathbf{D}_{BC}^4 \mathbf{X}^{n+1,*} + \boldsymbol{\lambda}^{n+1} \right) \\ &\quad + \mathbf{M}_{NL}^n \left(-\kappa_b \mathbf{D}_{BC}^4 \mathbf{X}^n + \boldsymbol{\lambda}^n \right) + \mathbf{M} \mathbf{f}^n \\ (\mathbf{K}^*)^n \boldsymbol{\lambda}^{n+1} &= \mathbf{0}, \end{aligned}$$

where $\mathbf{X}^{n+1,*} = \mathbf{X}^n + \Delta t \mathbf{K}^{n+1/2,*} \boldsymbol{\Omega}^{n+1/2}$.

- Actual fiber update is **strictly inextensible**

$$\boldsymbol{\tau}^{n+1} = \text{rotate}(\boldsymbol{\tau}^n, \Delta t \boldsymbol{\Omega}^n).$$

- \mathbf{f}^n contains other forces such as **cross-linkers** (can be stiff).
Flow is easy to add to the rhs.

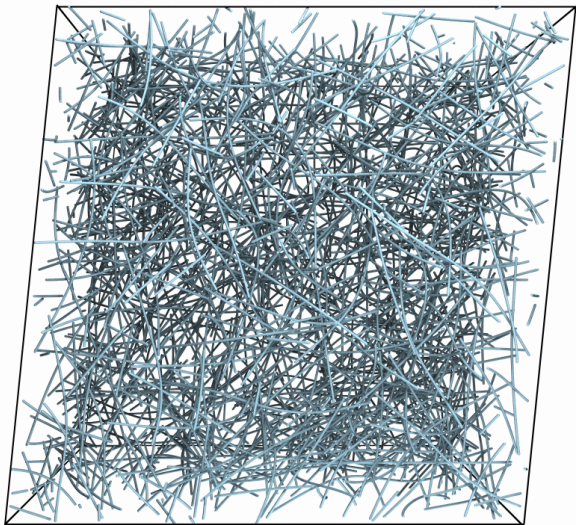
The gory details

- ① For dense suspensions, supplement L+NL splitting with additional **1-5 GMRES iterations** for stability.
- ② Evaluate long-ranged hydrodynamic interactions between Chebyshev nodes in **linear time** using *Positively Split Ewald* (PSE) method (FFT based for triply periodic), also works for **deformed/sheared unit cell** (Fiore et al. *J. Chem. Phys.* (2017)).
- ③ For **nearby fibers**, use specialized **near-singular quadrature** (af Klinteberg and Barnett. BIT Num. Math. 2020 [4]) to get 2-3 digits.
- ④ For intra-fiber hydro use specialized **slender-body quadrature** ala Anna Karin-Tornberg.

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Actin network/gel



Cross Linkers

- Cross linker (CL) between $\mathbf{X}^{(i)}(s_i^*)$ and $\mathbf{X}^{(j)}(s_j^*)$, with

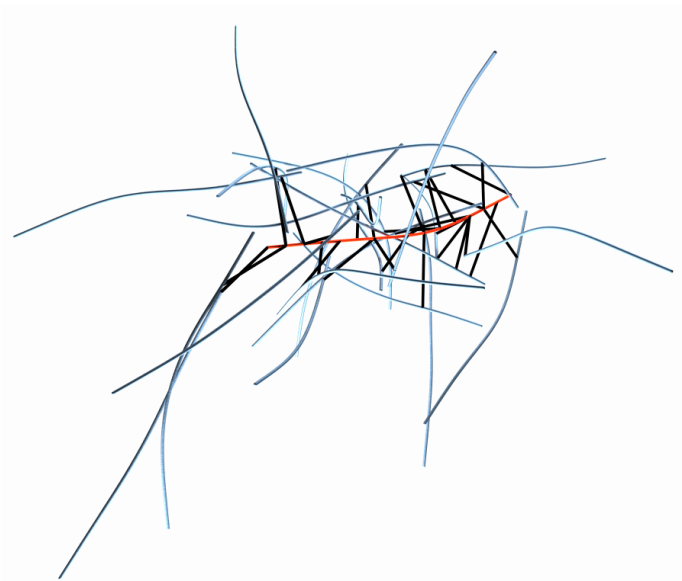
$$R = \left\| \mathbf{X}^{(i)}(s_i^*) - \mathbf{X}^{(j)}(s_j^*) \right\|$$

- Model cross-linker as just a spring with **Gaussian smoothing** to preserve spectral accuracy (std= $\sigma \sim 0.1L$):

$$\mathbf{f}^{(\text{CL},i)}(s) = -K_c \left(1 - \frac{\ell}{R} \right) \delta_\sigma(s - s_i^*) \int_0^L ds' \left(\mathbf{X}^{(i)}(s) - \mathbf{X}^{(j)}(s') \right) \delta_\sigma(s' - s_j^*)$$

- Cross linker is **force and torque-free**.
- Randomly generated dense network of CLs (16 attachment sites per site) to give about 12 CLs per fiber (elastic network).

Cross-linked network



Rheology

Apply linear shear flow $\mathbf{v}_0(x, y, z) = \dot{\gamma}_0 \cos(\omega t)y$ and measure the **visco-elastic stress** induced by the fibers and cross links:

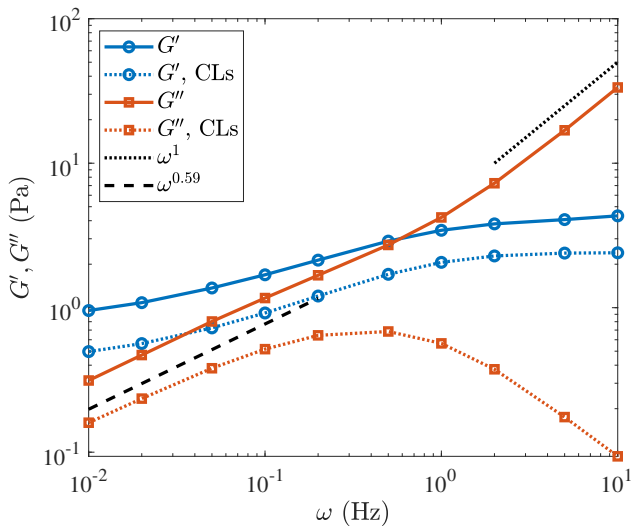
$$\boldsymbol{\sigma}^{(i)} = \frac{1}{V} \sum_{\text{fibers}} \int_0^L ds \mathbf{X}^i(s) (\mathbf{f}_b(s) + \boldsymbol{\lambda}(s))^T$$

$$\boldsymbol{\sigma}^{(CL)} = \frac{1}{V} \sum_{CLs=(i,j)} \int_0^L ds \left(\mathbf{X}^i(s) \mathbf{f}^{(CL,i)}(s) + \mathbf{X}^j(s) \mathbf{f}^{(CL,j)}(s) \right)$$

$$\frac{\sigma_{21}}{\gamma_0} = G' \sin(\omega t) + G'' \cos(\omega t) = \text{elastic} + \text{viscous.}$$

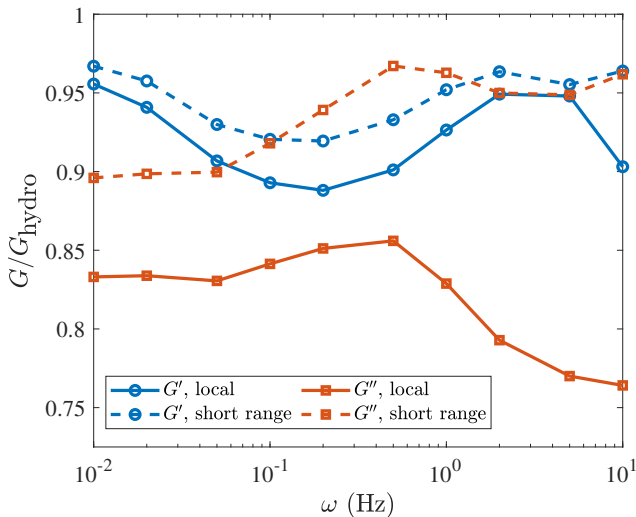
$$G' = \frac{2}{\gamma_0 T} \int_0^T \sigma_{21} \sin(\omega t) dt \quad G'' = \frac{2}{\gamma_0 T} \int_0^T \sigma_{21} \cos(\omega t) dt.$$

Viscoelastic moduli: Maxwell fluid



Elastic modulus G' and viscous modulus G'' for 700 fibers + 8400 CLs

Nonlocal hydrodynamics



Reduction in viscoelastic moduli with **only local drag** or **only inter-fiber nonlocal hydrodynamics**.

Rheology permanent CLs

- Network relaxation time $\tau_c \approx 0.5 - 1s$
- For $\omega^{-1} \gg \tau_c$
 - Quasi-steady; elastic solid
 - Small effect of nonlocal hydrodynamics ($\sim 10\%$)
- For $\omega^{-1} \approx \tau_c$.
 - $G'' \approx G'$
 - Max change in G' due to *inter-fiber* hydro
- For $\omega^{-1} \ll \tau_c$.
 - Fibers and CLs “frozen”; network behaves like a viscous fluid
 - $G'' \gg G'$; up to 25% change due to *intra-fiber* hydro.

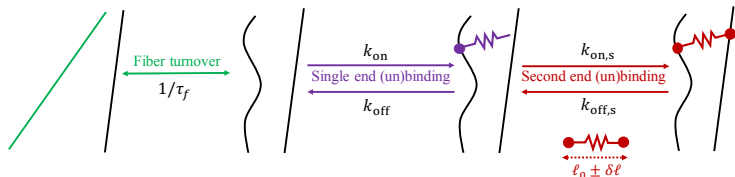
Dynamic cross linking

Kinetic Monte Carlo algorithm for cross linking:

- Discrete set of binding sites on each fiber (for efficiency).
- Doubly-bound CLs act as simple **elastic springs**.

Assumptions behind linking algorithm

- Diffusion of cross-linkers is fast (**diffusion-limited binding**)
- Four reactions between fibers and CL reservoir obey **detailed balance**



"Simulations of dynamically cross-linked actin networks..." O. Maxian et al, PLOS Comp. Bio., 17(12): e1009240, 2021 [[bioRxiv:2021.07.07.451453](https://doi.org/10.1371/journal.pcbi.1009240)] [5]

Temporal integrator

We use a **time splitting approach**:

- ① Turnover filaments over time Δt (rarely happens).
- ② Update cross linkers over time Δt .
- ③ Calculate $\mathbf{f}^{(CL)}(\mathbf{X})$ and solve

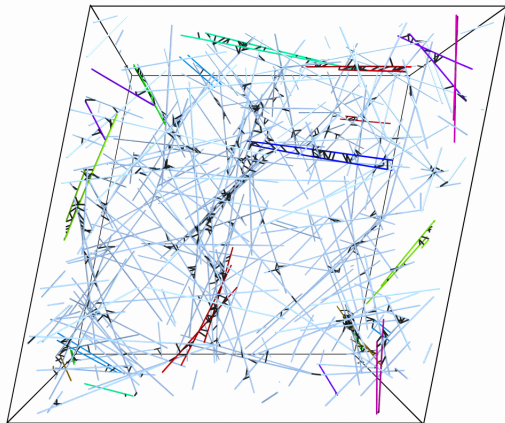
$$\frac{\partial \mathbf{X}}{\partial t} = \mathbf{M}(\mathbf{X}) \left[\mathbf{f}^{(\kappa)}(\mathbf{X}) + \mathbf{f}^{(CL)}(\mathbf{X}) + \boldsymbol{\lambda} \right]$$

and update \mathbf{X} over time Δt .

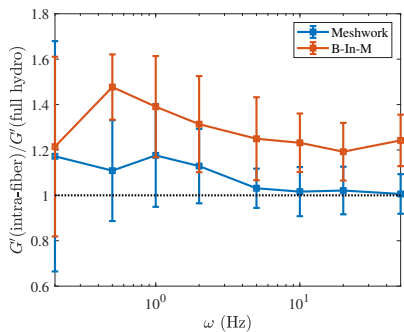
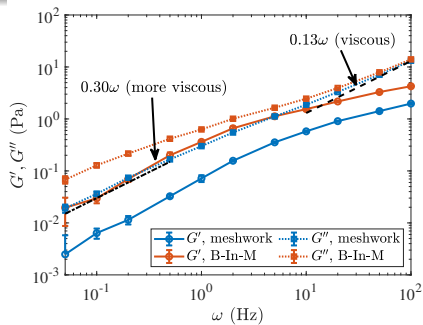
- ④ Translational and rotational **diffusion of rigid filaments** over time Δt (sometimes).

"Interplay between Brownian motion and cross-linking kinetics controls bundling dynamics in actin networks" by O. Maxian et al, in press Biophysical J., 2022
 [bioRxiv:021.09.17.460819] [6]

Dynamically cross-linked network



Rheology transient CLs



- Measured viscoelastic moduli of dynamically cross-linked networks **without** Brownian motion.
- For bundled networks, elastic modulus overestimated by $\approx 50\%$ without inter-fiber hydro, esp. long timescales.
- Fibers in bundles closer together: stress is reduced because **entrainment flows in bundle** make straining easier.

Outline

- 1 Motivation
- 2 Fibers in Stokes flow
 - Hydrodynamics
 - Adding twist
 - Inextensibility
- 3 Numerical Methods
- 4 Actin gels
- 5 Adding Brownian motion

Thermal fluctuations (Brownian Motion)

- **Rigid fibers** are “easy” [7] though so far we have only implemented *without* inter-fiber hydro [6].

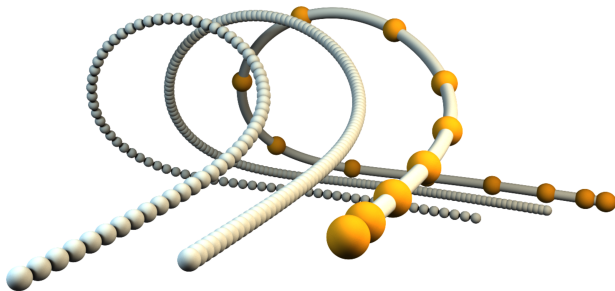
- Fluctuating hydrodynamics gives the fluctuating Stokes equations

$$\rho \partial_t \mathbf{v} + \nabla \pi = \eta \nabla^2 \mathbf{v} + \nabla \cdot \left(\sqrt{2\eta k_B T} \mathcal{W} \right) + \int_0^L ds \mathbf{f}(s, t) \delta_a(\mathbf{X}(s, t) - \mathbf{r}).$$

- The **thermal fluctuations** (Brownian motion of fiber) are driven by a white-noise **stochastic stress tensor** $\mathcal{W}(\mathbf{r}, t)$.
- Must first answer deep mathematical questions:
 - Can one make sense of the (multiplicative noise) **overdamped SPDE** for a Brownian curve?
 - Does the **Brownian stress** of the fiber converge in the continuum limit? (bending energy does not)

Brownian multiblob chains

For **Brownian blob-link chains** there are no mathematical issues so start there!



Fast constrained BD-HI for blob-link chains based on rotating unit link vectors including Brownian stress (Brennan Sprinkle, in progress)

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