

Numerical methods for inextensible slender fibers in Stokes flow

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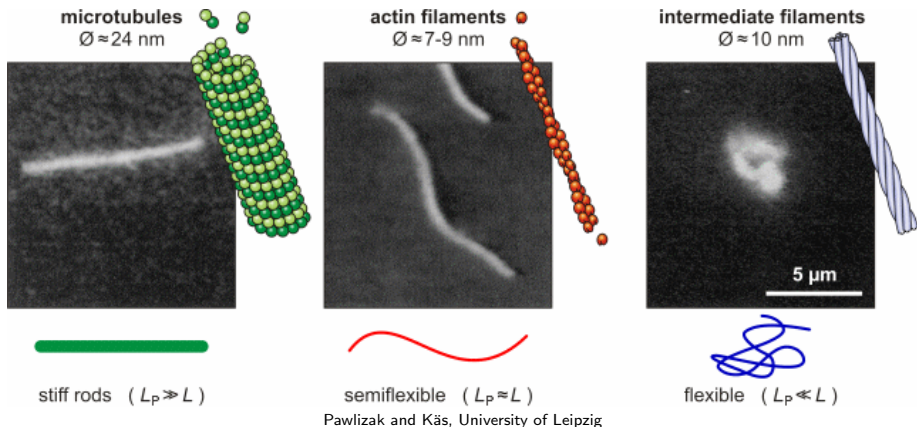
Outline

- 1 Motivation
- 2 Fibers in Stokes flow
- 3 Inextensibility
- 4 Numerical Methods
- 5 Actin gels
- 6 Future Challenges
 - Adding twist
 - Adding Brownian motion

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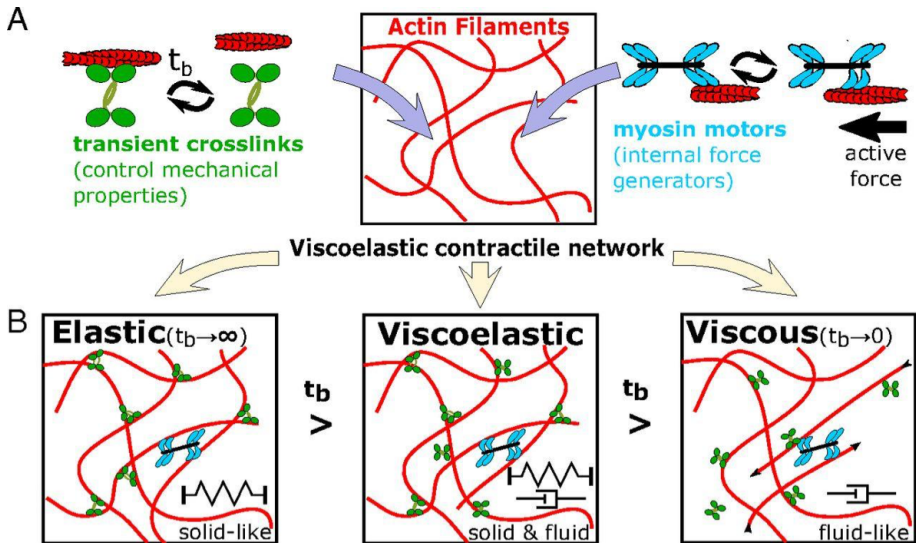
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Fibers involved in cell mechanics

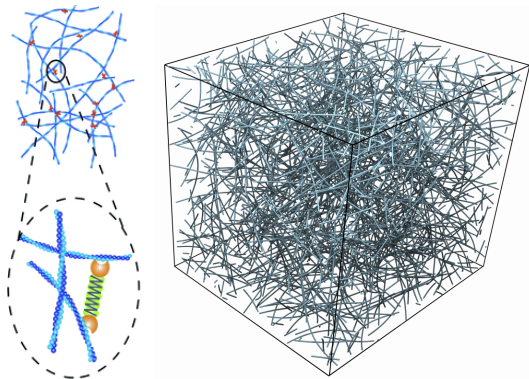


L_p = persistence length, L = fiber length, $a = \epsilon L$ = fiber radius,
 ϵ = slenderness ratio

Cytoskeleton rheology

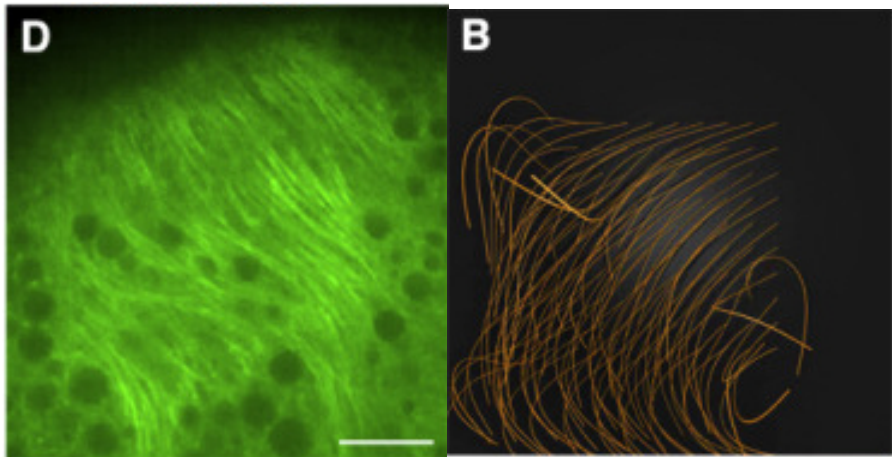
Ahmed and Betz. *PNAS*. (2015)

Cross-linked actin gels



- Very **slender semi-flexible fibers** (aspect ratio $10^2 - 10^4$) suspended in a **viscous solvent**.
- For now **cross linkers** modeled as simple elastic springs.
- **Periodic cyclically sheared** unit cell: **viscoelastic moduli**.

Does nonlocal hydrodynamics matter?



Monteith et al. Biophysics Journal. (2016)

Does nonlocal hydrodynamics matter?

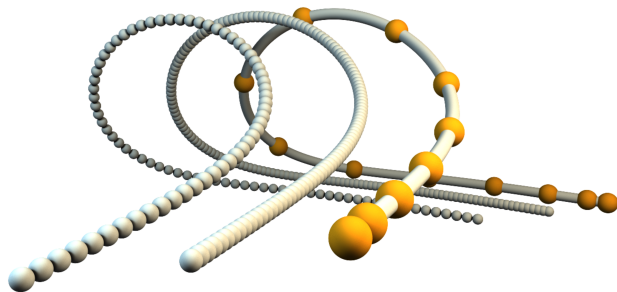
- Sometimes flows created by individual fibers add up constructively to produce **large-scale flows**, which advect network.
- For example, cytoplasmic streaming on previous slide or contraction of a myosin-actin gel (must expel liquid out).
- Flow is generated at scales of fiber thickness: **multiscale problem**.
- Role of **long-ranged (nonlocal) hydrodynamics** unclear for rheology of cross-linked actin gels.
- For background consult:
Dynamics of Flexible Fibers in Viscous Flows and Fluids, Annual Review of Fluid Mechanics 51:539, Olivia du Roure, Anke Lindner, Ehssan N. Nazockdast, and Michael J. Shelley

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Fiber Representation

Simple approach is to represent a fiber as a **discrete chain** of beads/blobs: **multiblob model**

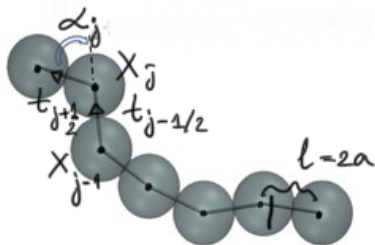


More efficient approach is to represent a fibers as **continuum curve**

O. Maxian, A. Mogilner and A. Donev, **ArXiv:2007.11728**

An integral-based spectral method for inextensible slender fibers in Stokes flow [1]

Inextensible multilob chains



Worm-like polymer chain

- Inextensibility: $\|\mathbf{X}_{j+1} - \mathbf{X}_j\| = l \sim a$ (e.g., a or $2a$).
- Tangent vectors:

$$\boldsymbol{\tau}_{j+1/2} = (\mathbf{X}_{j+1} - \mathbf{X}_j) / l$$
- Bending angles:

$$\cos \alpha_j = \boldsymbol{\tau}_{j+1/2} \cdot \boldsymbol{\tau}_{j-1/2}$$
- Elastic energy (bending modulus κ_b)

$$E_b = \frac{2\kappa_b}{l} \sum_{j=1}^{N-1} \sin^2 \left(\frac{\alpha_j}{2} \right)$$

Inextensible continuum fibers

- Persistence length due to thermal fluctuations $\xi = 2\kappa_b / (k_B T) \gg l$ gives us a **continuum limit**, $\alpha_j \ll 1$.
- Fiber centerline $\mathbf{X}(s)$ where the **arc length** $0 \leq s \leq L$.
- The tangent vector is $\boldsymbol{\tau} = \partial \mathbf{X} / \partial s = \mathbf{X}_s$, and the **fibers are inextensible**,

$$\boldsymbol{\tau}(s, t) \cdot \boldsymbol{\tau}(s, t) = 1 \quad \forall (s, t).$$

- Bending energy functional is integral of inverse curvature squared:

$$E_b(\mathbf{X}) = \frac{2\kappa_b}{l} \sum_{j=1}^{N-1} \left(\frac{\alpha_j}{2}\right)^2 \quad \Rightarrow \quad E_b[\mathbf{X}(\cdot)] = \frac{\kappa_b}{2} \int ds \|\mathbf{X}_{ss}(s)\|^2$$

Bending elasticity

- Bending force $\mathbf{F}_j^{(b)}$ on each blob j in the interior gives us **elastic force density** $\mathbf{f}_b(s, t)$

$$\mathbf{F}_j^{(b)} = -\frac{\partial E_b}{\partial \mathbf{X}_j} = \frac{\kappa_b}{l^3} (-\mathbf{X}_{j-2} + 4\mathbf{X}_{j-1} - 6\mathbf{X}_j + 4\mathbf{X}_{j+1} - \mathbf{X}_{j+2})$$

$$\mathbf{F}_b \approx -l\kappa_b \mathbf{D}^4 \mathbf{X} \quad \Rightarrow \quad \mathbf{f}_b = -\frac{\delta E_{\text{bend}}}{\delta \mathbf{X}} = -\kappa_b \mathbf{X}_{ssss}$$

- Endpoints naturally handled discretely, giving in continuum natural BCs for **free fibers**:

$$\mathbf{X}_{ss}(0/L) = 0, \quad \mathbf{X}_{sss}(0/L) = 0.$$

- Tensions** $T_{j+1/2} \rightarrow T(s)$ are **unknown** and resist stretching,

$$\Lambda_i = T_{i+1/2} \boldsymbol{\tau}_{i+1/2} - T_{i-1/2} \boldsymbol{\tau}_{i-1/2} \quad \Rightarrow \quad \boldsymbol{\lambda} = (T\boldsymbol{\tau})_s.$$

Fluid dynamics

- For multiblob chains in **Stokes flow**, fluid velocity $\mathbf{v}(\mathbf{r}, t)$ satisfies $\nabla \cdot \mathbf{v} = \mathbf{0}$ and

$$\nabla \pi = \eta \nabla^2 \mathbf{v} + \sum_j \mathbf{F}_j \delta_a(\mathbf{X}_j - \mathbf{r}),$$

where δ_a is a **regularized delta/blob function** whose width is proportional to a , and

$$\mathbf{F} = -l\kappa_b \mathbf{D}^4 \mathbf{X} + \Lambda$$

- Blobs/fiber are advected by fluid

$$\mathbf{U}_j = d\mathbf{X}_j/dt = \int d\mathbf{r} \mathbf{v}(\mathbf{r}, t) \delta_a(\mathbf{X}_j - \mathbf{r}).$$

- Continuum limit is obvious

$$\nabla \pi(\mathbf{r}, t) = \eta \nabla^2 \mathbf{v}(\mathbf{r}, t) + \int_0^L ds \mathbf{f}(s, t) \delta_a(\mathbf{X}(s, t) - \mathbf{r})$$

$$\mathbf{U}(s, t) = \partial_t \mathbf{X}(s, t) = \int d\mathbf{r} \mathbf{v}(\mathbf{r}, t) \delta_a(\mathbf{X}(s, t) - \mathbf{r})$$

$$\mathbf{f} = -\kappa_b \mathbf{X}_{ssss} + \lambda$$

Multiblob chains in Stokes flow

- We can (temporarily) eliminate the fluid velocity to write an equation for **fiber only**.
- Define the positive semi-definite **hydrodynamic kernel**

$$\mathcal{R}(\mathbf{r}_1, \mathbf{r}_2) = \int \delta_a(\mathbf{r}_1 - \mathbf{r}') \mathbb{G}(\mathbf{r}', \mathbf{r}'') \delta_a(\mathbf{r}_2 - \mathbf{r}'') d\mathbf{r}' d\mathbf{r}'',$$

where \mathbb{G} is the Green's function for (periodic) Stokes flow.

- Define $\mathbf{M}(\mathbf{X}) \succeq \mathbf{0}$ to be the symmetric positive semidefinite (SPD) **mobility matrix** with blocks

$$\mathbf{M}_{ij}(\mathbf{X}_i, \mathbf{X}_j) = \mathcal{R}(\mathbf{X}_i, \mathbf{X}_j) = \mathcal{R}(\mathbf{X}_i - \mathbf{X}_j).$$

- Discrete dynamics = **inextensibility** +

$$\mathbf{U} = d\mathbf{X}/dt = \mathbf{M}(\mathbf{X}) \mathbf{F}(\mathbf{X}) = \mathbf{M}(-l\kappa_b \mathbf{D}^4 \mathbf{X} + \mathbf{\Lambda})$$

Inextensible fibers in Stokes flow

- Define a positive semidefinite **mobility operator**

$$(\mathcal{M}[\mathbf{X}(\cdot)] \mathbf{f}(\cdot))(s) = \int_0^L ds' \mathcal{R}(\mathbf{X}(s), \mathbf{X}(s')) \mathbf{f}(s')$$

- Continuum dynamics is a **non-local PDE**

$$\mathbf{U} = \mathbf{X}_t = \mathcal{M}[\mathbf{X}] (-\kappa_b \mathbf{X}_{ssss} + \boldsymbol{\lambda})$$

$$\boldsymbol{\tau}(s, t) \cdot \boldsymbol{\tau}(s, t) = 1 \quad \forall (s, t).$$

- Is this PDE well-posed (weak, strong)? Since $\boldsymbol{\lambda}$ only appears inside spatial integrals, this is a sort of first-kind integral equation.
- Recent work by Ohm and Mori defines a “**slender-body PDE**” that is *probably* well-posed (not proven yet for inextensible fibers or for cylindrical fibers with free ends) but too difficult for computation.

Rotne-Prager-Yamakawa kernel

$$\mathcal{R}(\mathbf{r}_1, \mathbf{r}_2) = \int \delta_a(\mathbf{r}_1 - \mathbf{r}') \mathbb{G}(\mathbf{r}', \mathbf{r}'') \delta_a(\mathbf{r}_2 - \mathbf{r}'') d\mathbf{r}' d\mathbf{r}''$$

- Taking the regularization kernel and unbounded Stokes flow

$$\delta_a(\mathbf{r}) = (4\pi a^2)^{-1} \delta(r - a)$$

gives the **Rotne-Prager-Yamakawa (RPY) kernel**

$$\mathcal{R}(\mathbf{r}) = \begin{cases} (8\pi\eta)^{-1} \left(\mathcal{S}(\mathbf{r}) + \frac{2a^2}{3} \mathcal{D}(\mathbf{r}) \right), & r > 2a \\ (6\pi a\eta)^{-1} \left[\left(1 - \frac{9r}{32a} \right) \mathbf{I} + \left(\frac{3r}{32a} \right) \frac{\mathbf{r} \otimes \mathbf{r}}{r^2} \right], & r \leq 2a \end{cases}$$

$$\mathcal{S}(\mathbf{r}) = \frac{1}{8\pi\eta r} (\mathbf{I} + \hat{\mathbf{r}}\hat{\mathbf{r}}^T) \equiv \mathbb{G}, \quad \text{and} \quad \mathcal{D}(\mathbf{r}) = \frac{1}{8\pi\eta r^3} (\mathbf{I} - \hat{\mathbf{r}}\hat{\mathbf{r}}^T)$$

Matched asymptotics

$$(\mathcal{M}[\mathbf{X}(\cdot)] \mathbf{f}(\cdot))(s) = \int_0^L ds' \mathcal{R}(\mathbf{X}(s) - \mathbf{X}(s')) \mathbf{f}(s')$$

- **Matched asymptotics** gives (away from endpoints)

$$\begin{aligned} (\mathcal{M} \mathbf{f})(s) &\approx (\mathcal{M}_{\text{SBT}} \mathbf{f})(s) = (\mathcal{M}_{\text{loc}} \mathbf{f})(s) + (\mathcal{M}_{\text{FP}} \mathbf{f})(s) = \\ &= \frac{1}{8\pi\mu} \left(\log \left(\frac{(L-s)s}{4a^2} \right) (\mathbf{I} + \boldsymbol{\tau}(s)\boldsymbol{\tau}(s)^T) + 4\mathbf{I} \right) \mathbf{f}(s) \\ &\quad + \frac{1}{8\pi\mu} \int_0^L ds' \left(\boldsymbol{\mathcal{S}}(\mathbf{X}(s) - \mathbf{X}(s')) \mathbf{f}(s') - \left(\frac{\mathbf{I} + \boldsymbol{\tau}(s)\boldsymbol{\tau}(s)^T}{|s-s'|} \right) \mathbf{f}(s) \right) \end{aligned}$$

- For a special choice of blob radius $a = (e^{3/2}/4) \epsilon L = 1.12\epsilon L$, this formula matches the widely-used **Slender Body Theory** (SBT).
- Our approach automatically works for **multiple fibers**, and also gives us a natural **regularization of the endpoints** (not shown).

Slender body theory

$$\mathcal{M} = \mathcal{M}_{\text{loc}} + \mathcal{M}_{\text{FP}} = \mathcal{O} \left(\log \left(\frac{(L-s)s}{a^2} \right) \right) + \mathcal{O}(1)$$

- SBT is great for numerics since it involves **quadratures** that can be computed accurately for smooth \mathbf{f} to **spectral accuracy**.
- Problem 1: The local drag term is logarithmically **singular at endpoints** for cylindrical fibers.
Many use (unphysical) **ellipsoidal fibers**: $\mathcal{M}_{\text{loc}} = \mathcal{O}(\log(L/a))$.
- Problem 2: The finite-part mobility \mathcal{M}_{FP} has **spurious negative eigenvalues** for high spatial frequencies, so \mathcal{M}_{SBT} is **not SPD**, and equations are definitely **not well posed**.
Previous works starting with Tornberg+Shelley [2] use **artificial regularization** of the integrand in \mathcal{M}_{FP} .

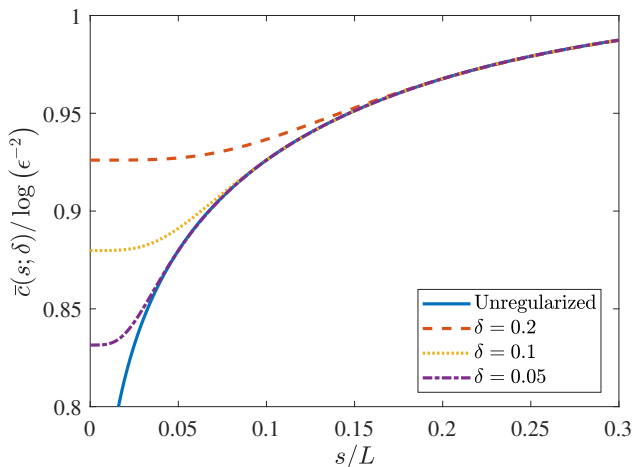
Limitations of slender body theory

- Problem 1 compounds problem 2, and for fibers of slenderness $\epsilon \sim 10^{-2}$ all of SBT seems to break down.
- Problem 2 solution: One can avoid matched asymptotics entirely by constructing **special quadrature methods** for the RPY kernel (using ideas of af Klinteberg, Barnett, Tornberg).
- Problem 1 temporary “solution”:
Make fibers **tapered near the endpoints** ($\delta \sim 0.05 - 0.1 \gg \epsilon$)



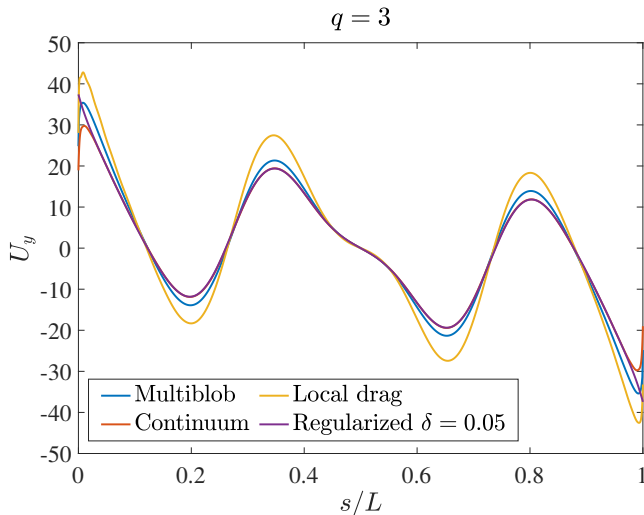
Regularization of end points

$$(\mathcal{M}_{\text{loc}} \mathbf{f})(s) \sim c(s) (\mathbf{I} + \boldsymbol{\tau}(s)\boldsymbol{\tau}(s)^T) \mathbf{f}(s), \quad \text{where} \quad c(s) \sim \log \left(\frac{(L-s)s}{a(s)^2} \right)$$



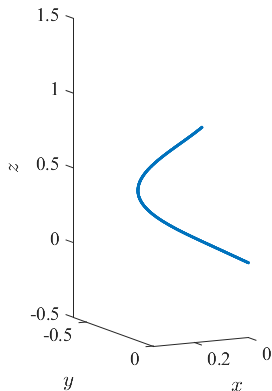
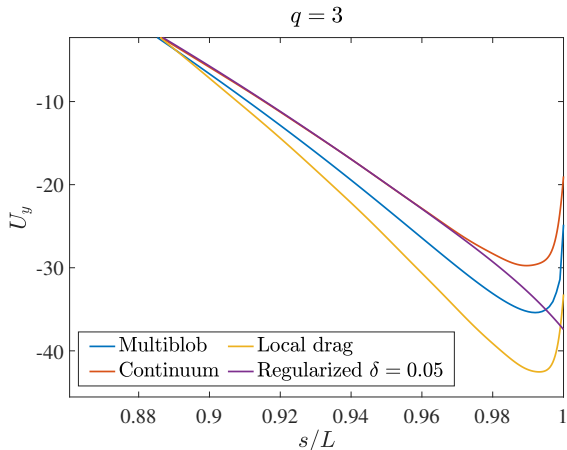
Note: For ellipsoidal fibers $c(s)$ is constant ($= 1$ in this plot).

Cylindrical fibers



Velocity at $t = 0$ for fiber with $\epsilon = 10^{-3}$ relaxing due to bending elasticity.

Cylindrical endpoints



Lack of smoothness in the solution near the endpoints – our **endpoint regularization** removes that problem.

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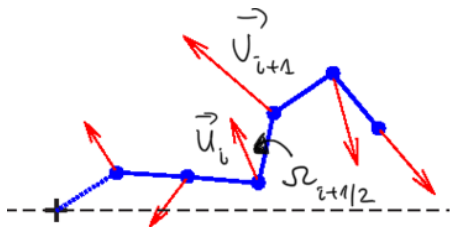
Tension equation

$$\mathbf{X}_t = \mathcal{M}[\mathbf{X}] (-\kappa_b \mathbf{X}_{ssss} + \lambda) \quad \text{and} \quad \lambda = (T\boldsymbol{\tau})_s$$

- Traditional approach (Tornberg+Shelley) is to solve **tension equation**

$$\boldsymbol{\tau} \cdot \boldsymbol{\tau} = \mathbf{X}_s \cdot \mathbf{X}_s = 1 \quad \Rightarrow \quad (\mathbf{X}_t)_s \cdot \mathbf{X}_s = 0 \quad \text{non-local BVP}$$
- Tension equation is linear in $T(s)$ but very nonlinear in \mathbf{X} and its derivatives, causing **aliasing issues**.
- Method does not strictly enforce inextensibility numerically, requiring adding a **penalty for stretching**.
- To solve these problems, let us first go back to multiblobs for simplicity, and then take continuum limits.

Inextensible motions



$$\frac{\mathbf{U}_i - \mathbf{U}_{i-1}}{\Delta s} = \Omega_{j+1/2} \times \boldsymbol{\tau}_{j+1/2} \quad \Rightarrow$$

$$\mathbf{U} = \mathbf{K} \Omega^\perp = \left[\mathbf{U}_0, \dots, \mathbf{U}_0 + \Delta s \sum_{j=0}^{i-1} \Omega_{j+1/2}^\perp \times \boldsymbol{\tau}_{j+1/2}, \dots \right] \rightarrow$$

$$\left(\boldsymbol{\kappa} [\mathbf{X}(\cdot)] \Omega^\perp(\cdot) \right) (s) = \mathbf{U}(s) = \mathbf{U}(0) + \int_0^s ds' \left(\Omega^\perp(s') \times \boldsymbol{\tau}(s') \right).$$

Principle of virtual work

- **Principle of virtual work:** Constraint forces should do no work for any inextensible motion of the fiber:

$$\mathbf{\Lambda}^T \mathbf{U} = (\mathbf{K}^T \mathbf{\Lambda})^T \mathbf{\Omega}^\perp = 0 \quad \forall \mathbf{\Omega}^\perp \quad \Rightarrow \quad \mathbf{K}^T \mathbf{\Lambda} = \mathbf{0}$$

$$\mathbf{K}^T \mathbf{\Lambda} = \left[\sum_{j=0}^N \mathbf{\Lambda}_j, \dots, \Delta s \left(\sum_{j=i}^N \mathbf{\Lambda}_j \right) \times \boldsymbol{\tau}_{i+1/2}, \dots \right] \rightarrow$$

$$(\mathcal{K}^* [\mathbf{X}(\cdot)] \boldsymbol{\lambda}(\cdot))(s) = \left[\int_0^L ds' \boldsymbol{\lambda}(s'), \left(\int_s^L ds' \boldsymbol{\lambda}(s') \right) \times \boldsymbol{\tau}(s) \right] = 0 \quad \forall s.$$

- We can express this in terms of tension

$$\forall s \quad \int_s^L ds' \boldsymbol{\lambda}(s') = -T(s) \boldsymbol{\tau}(s) \quad \Rightarrow \quad \boldsymbol{\lambda} = (T \boldsymbol{\tau})_s$$

but the principle of virtual work is an **integral constraint** rather than a pointwise constraint.

Continuum equations

- New **weak formulation of inextensibility** constraint:

$$\mathbf{X}_t = \mathcal{K}[\mathbf{X}] \Omega^\perp = \mathcal{M}[\mathbf{X}] (-\kappa_b \mathbf{X}_{ssss} + \lambda)$$

$$\mathcal{K}^*[\mathbf{X}] \lambda = \mathbf{0}$$

$$\partial_t \boldsymbol{\tau} = \Omega^\perp \times \boldsymbol{\tau}$$

$$\mathbf{X}(s, t) = \mathbf{X}(0, t) + \int_0^s ds' \boldsymbol{\tau}(ds', t)$$

- Two improvements:
 - Evolve tangent vector $\boldsymbol{\tau}$ rather than \mathbf{X} : **strictly inextensible**.
 - Impose tension equation **weakly** rather than pointwise.

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Chebyshev discretization

- Choose normal vectors $\mathbf{n}_{1/2} \perp \boldsymbol{\tau}$ (arbitrary):

$$\partial_t \boldsymbol{\tau} = \boldsymbol{\Omega}^\perp \times \boldsymbol{\tau} = g_1(s) \mathbf{n}_1(s) + g_2(s) \mathbf{n}_2(s)$$

- Expand all functions into a **truncated Chebyshev series** on a grid of N nodes using $T_k(s)$ as a basis for L_2 :

$$g_1(s) = \sum_{j=0}^{N-1} \alpha_{1j} T_j(s) \quad \text{kinematic vars } \boldsymbol{\alpha} = \{\mathbf{U}(0), \alpha_{1j}, \alpha_{2j}\}$$

- Simple change of integration vars gives

$$\mathbf{U} = \boldsymbol{\kappa} [\mathbf{X}] \boldsymbol{\alpha} = \mathbf{U}(0) + \sum_{j=0}^{N-1} \int_0^s ds' (\alpha_{1j} T_j(s') \mathbf{n}_1(s') + \alpha_{2j} T_j(s') \mathbf{n}_2(s'))$$

Chebyshev discretization contd.

- Principle of virtual work says $\forall j$

$$\mathcal{K}^*[\mathbf{X}] \lambda = \begin{pmatrix} \int_0^L \lambda(s) ds \\ \int_0^L ds \lambda(s) \cdot \int_0^s ds' T_j(s') \mathbf{n}_{1/2}(s') \end{pmatrix} := \mathbf{0}$$

- **Collocation discretization** of mobility equation gives a **saddle point system** for λ and α ,

$$\begin{pmatrix} -\mathbf{M}(\mathbf{X}) & \mathbf{K}(\mathbf{X}) \\ \mathbf{K}^*(\mathbf{X}) & \mathbf{0} \end{pmatrix} \begin{pmatrix} \lambda \\ \alpha \end{pmatrix} = \begin{pmatrix} \mathbf{M}(\mathbf{X})(-\kappa_b \mathbf{D}_{BC}^4 \mathbf{X}) \\ \mathbf{0} \end{pmatrix}$$

but should try Galerkin in the future.

- Bending elasticity+BCs discretized using **rectangular collocation**
Driscoll and Hale. *IMA J. Numer. Anal.* (2016).

Temporal discretization

- Use multistep **extrapolation** for nonlinear terms:

$$\mathbf{X}^{n+1/2,p} = \frac{3}{2}\mathbf{X}^n - \frac{1}{2}\mathbf{X}^{n-1}$$

$$\lambda^{n+1/2,p} = 2\lambda^{n-1/2} - \lambda^{n-3/2}.$$

- Split** mobility into **local and non-local** parts, $\mathbf{M} = \mathbf{M}_L + \mathbf{M}_{NL}$:

$$\mathbf{K}^{n+1/2,p} \alpha^{n+1/2} = \mathbf{M}_L^{n+1/2,p} \left(-\frac{\kappa_b}{2} \mathbf{D}_{BC}^4 (\mathbf{X}^n + \mathbf{X}^{n+1,*}) + \lambda^{n+1/2} \right)$$

$$+ \mathbf{M}_{NL}^{n+1/2,p} \left(-\kappa_b \mathbf{D}_{BC}^4 \mathbf{X}^{n+1/2,p} + \lambda^{n+1/2,p} \right)$$

$$(\mathbf{K}^*)^{n+1/2,p} \lambda^{n+1/2} = \mathbf{0},$$

where $\mathbf{X}^{n+1,*} = \mathbf{X}^n + \Delta t \mathbf{K}^{n+1/2,*} \alpha^{n+1/2}$.

- Actual fiber update is **strictly inextensible**

$$\boldsymbol{\tau}^{n+1} = \text{rotate} \left(\boldsymbol{\tau}^n, \Delta t \boldsymbol{\Omega}^{n+1/2,p} \right).$$

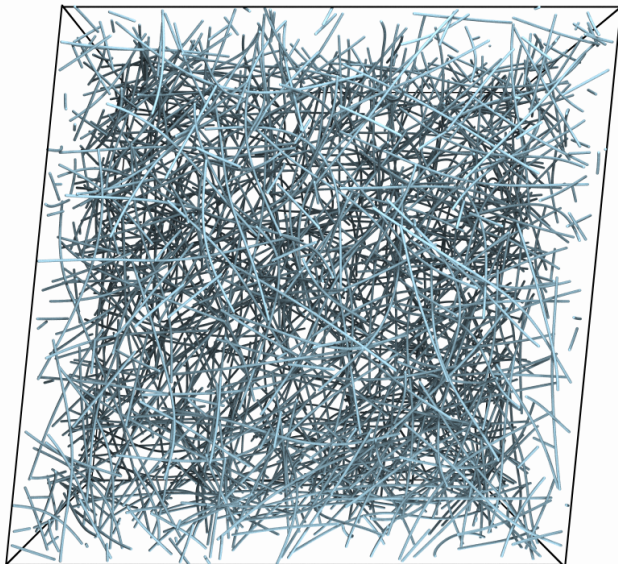
The gory details

- ① For dense suspensions, supplement 2nd order temporal method with additional **1-5 GMRES iterations** for stability.
- ② Evaluate long-ranged hydrodynamic interactions between Chebyshev nodes in linear time using **Positively Split Ewald** (PSE) method (FFT based for triply periodic), also works for **deformed/sheared unit cell** (Fiore *et al.* *J. Chem. Phys.* (2017) [3]).
Future work: Ewald methods with other BCs.
- ③ For **nearby fibers**, use specialized **near-singular quadrature** (af Klinteberg and Barnett. *BIT Num. Math.* 2020 [4]) to get 2-3 digits.
- ④ For finite-part self interaction of one fiber with itself use specialized **quadrature with singularity-removal** by Anna Karin-Tornberg.
Future work: Develop fast accurate quadratures for RPY kernel to *avoid* matched asymptotics (SBT).

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Actin network/gel



Cross Linkers

- Cross linker (CL) between $\mathbf{X}^{(i)}(s_i^*)$ and $\mathbf{X}^{(j)}(s_j^*)$, with

$$R = \left\| \mathbf{X}^{(i)}(s_i^*) - \mathbf{X}^{(j)}(s_j^*) \right\|$$

- Model cross-linker as just a spring with **Gaussian smoothing** to preserve spectral accuracy (std = $\sigma \sim 0.1L$):

$$\mathbf{f}^{(\text{CL},i)}(s) = -K_c \left(1 - \frac{\ell}{R} \right) \delta_\sigma(s - s_i^*) \int_0^L ds' \left(\mathbf{X}^{(i)}(s) - \mathbf{X}^{(j)}(s') \right) \delta_\sigma(s' - s_j^*)$$

- Cross linker is force and torque-free.
- Randomly generated dense network of CLs (16 attachment sites per site) to give about 12 CLs per fiber (elastic network).
- Future work: Allow for dynamic binding/unbinding of CLs, reduce smoothing σ , treat CL elasticity implicitly.

Cross-linked network



Rheology

Apply linear shear flow $\mathbf{v}_0(x, y, z) = \dot{\gamma}_0 \cos(\omega t)y$ and measure the **visco-elastic stress** induced by the fibers and cross links:

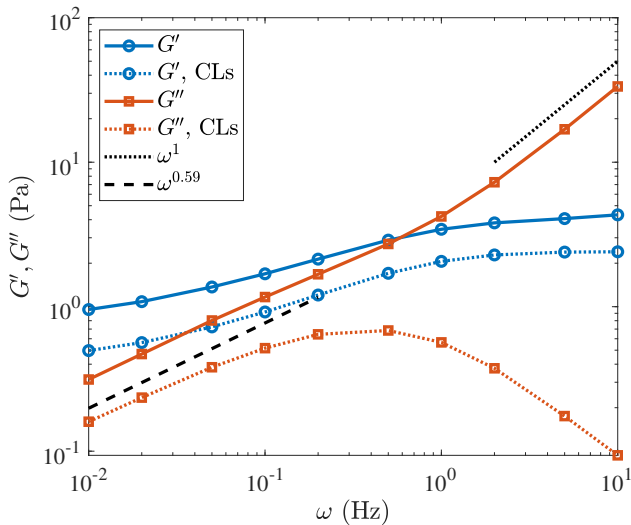
$$\boldsymbol{\sigma}^{(i)} = \frac{1}{V} \sum_{\text{fibers}} \int_0^L ds \mathbf{X}^i(s) (\mathbf{f}_b(s) + \boldsymbol{\lambda}(s))^T$$

$$\boldsymbol{\sigma}^{(CL)} = \frac{1}{V} \sum_{CLs=(i,j)} \int_0^L ds \left(\mathbf{X}^i(s) \mathbf{f}^{(CL,i)}(s) + \mathbf{X}^j(s) \mathbf{f}^{(CL,j)}(s) \right)$$

$$\frac{\sigma_{21}}{\gamma_0} = G' \sin(\omega t) + G'' \cos(\omega t) = \text{elastic} + \text{viscous.}$$

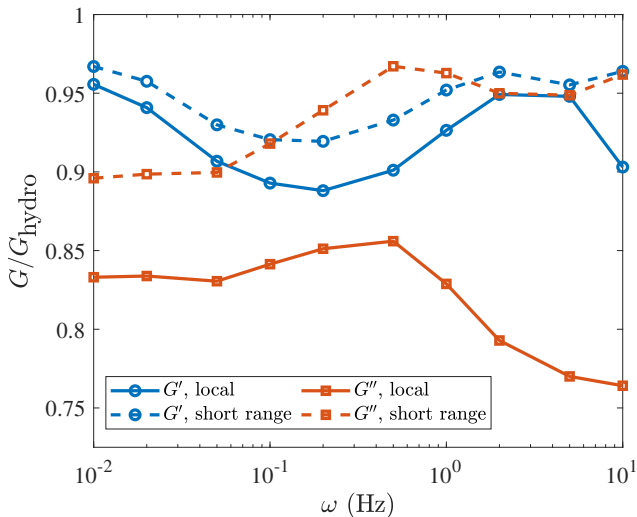
$$G' = \frac{2}{\gamma_0 T} \int_0^T \sigma_{21} \sin(\omega t) dt \quad G'' = \frac{2}{\gamma_0 T} \int_0^T \sigma_{21} \cos(\omega t) dt.$$

Viscoelastic moduli



Elastic modulus G' and viscous modulus G'' for 700 fibers + 8400 CLs

Nonlocal hydrodynamics



Reduction in viscoelastic moduli with **only local drag** or **only inter-fiber nonlocal hydrodynamics**.

Rheology summary

- Network relaxation time $\tau_c \approx 0.5 - 1s$
- For $\omega^{-1} \gg \tau_c$
 - Quasi-steady; elastic solid
 - Small effect of nonlocal hydrodynamics ($\sim 10\%$)
- For $\omega^{-1} \approx \tau_c$.
 - $G'' \approx G'$
 - Max change in G' due to *inter-fiber* hydro
- For $\omega^{-1} \ll \tau_c$.
 - Fibers and CLs “frozen”; network behaves like a viscous fluid
 - $G'' \gg G'$; up to 25% change due to *intra-fiber* hydro.

Outline

- 1 Motivation
- 2 Fibers in Stokes flow
- 3 Inextensibility
- 4 Numerical Methods
- 5 Actin gels
- 6 Future Challenges**
 - Adding twist
 - Adding Brownian motion

Twist

- For given force densities $\mathbf{f}(s, t)$ and **parallel torque** densities $m(s, t)$ along the fiber centerlines,

$$\nabla \pi = \eta \nabla^2 \mathbf{v} + \int_0^L ds \left[\mathbf{f}(s) + m(s) \boldsymbol{\tau}(s) \frac{\nabla}{2} \times \right] \delta_a(\mathbf{X}(s) - \mathbf{r}),$$

$$\Omega^{\parallel}(s) = \boldsymbol{\tau}(s) \cdot \int d\mathbf{r} \frac{\nabla}{2} \times \mathbf{v}(\mathbf{r}, t) \delta_a(\mathbf{X}(s) - \mathbf{r})$$

- Open question: Should fiber exert **perpendicular torques** on the fluid (and vice versa)?
- Previous work using multiblob-type methods makes \mathbf{m} a 3D vector (Peskin, Lim, Olson, Keaveny) and uses **Kirchhoff rod theory** (triad based) but we use scalar twist angle (inspired by work in group of Jorn Dunkel).

Bishop frame

- To each point along the fiber we attach an orthonormal triad $\mathbf{B}(s) = [\boldsymbol{\tau}(s), \mathbf{a}(s), \mathbf{b}(s)]$ called the **Bishop frame**, which satisfies the *no-twist condition*:

$$\mathbf{a}_s \cdot \mathbf{b} = 0 \quad \Rightarrow \quad \partial_s \mathbf{a} = (\boldsymbol{\tau} \times \boldsymbol{\tau}_s) \times \mathbf{a}$$

- Represent the **twist** of the i -th fiber by the angle $\theta(s)$ between the material frame of the cross section of the fiber and the Bishop cross section.

$$\begin{aligned} \mathbf{f} &= -\kappa_b \mathbf{X}_{SSSS} + \kappa_t (\theta_s (\boldsymbol{\tau} \times \boldsymbol{\tau}_s))_s + \boldsymbol{\lambda}, \\ m &= \kappa_T \theta_{SS} \end{aligned}$$

- Bishop frame evolves even if $\Omega^{\parallel} = 0$,

$$\partial_t \theta(s, t) = \partial_t \theta(s=0, t) + \int_0^s ds' \Omega_s(s', t) \cdot \boldsymbol{\tau}(s', t).$$

Why twist is hard

- Can we solve Bishop frame ODE efficiently with spectral methods?
- Temporal integration is challenging because of **extreme stiffness**: twist relaxation much faster than bend relaxation.
Maybe twist is always in **quasi-equilibrium**?
- When **does twist matter**?
Flagella, formins twisting growing actin filaments, macroscopic chirality in cells, and ?

Thermal fluctuations (Brownian Motion)

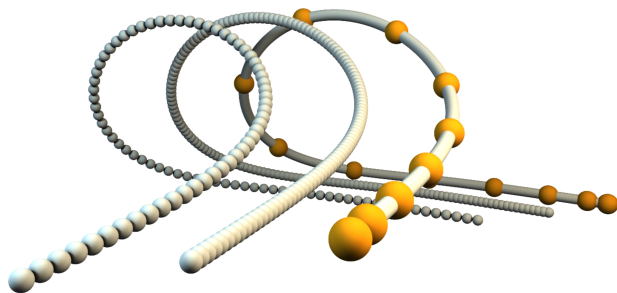
- Fluctuating hydrodynamics gives the fluctuating Stokes equations

$$\rho \partial_t \mathbf{v} + \nabla \pi = \eta \nabla^2 \mathbf{v} + \nabla \cdot \left(\sqrt{2\eta k_B T} \mathcal{W} \right) + \int_0^L ds \mathbf{f}(s, t) \delta_a(\mathbf{X}(s, t) - \mathbf{r}).$$

- The **thermal fluctuations** (Brownian motion of fiber) are driven by a white-noise **stochastic stress tensor** $\mathcal{W}(\mathbf{r}, t)$.
- Open mathematical question:
 - What is the **overdamped** limit $\eta/\rho \rightarrow \infty$ (steady Stokes)?
 - Can one even write a **multiplicative noise SPDE** for the fiber motion that makes mathematical sense?

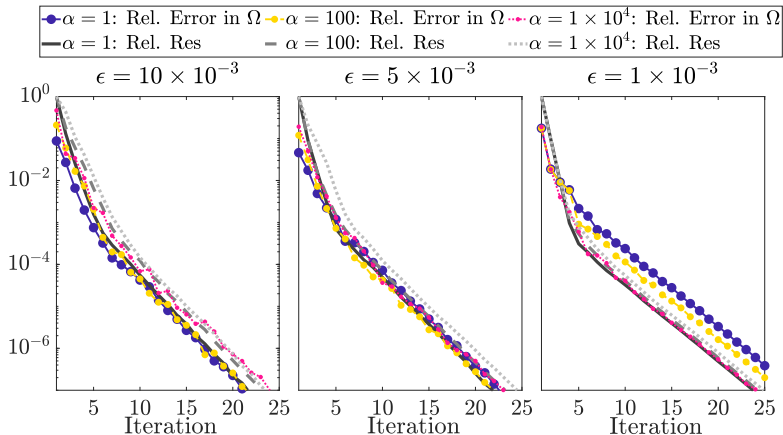
Brownian multiblob chains

For **Brownian multiblob chains** there are no mathematical issues so start there!



Multiblob chains: Linear Algebra

Since multiblobs have lots of DOFs per fiber, LA matters



GMRES convergence for implicit solver for a curved fiber, using **local-drag SBT** as a **preconditioner** (from B. Sprinkle).

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